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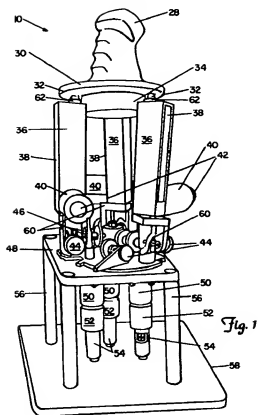
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(24) Hand controller.

(75) An active virtual pivot hand controller (10) using motors to control reflective forces and torques. Degree of freedom parameters, stops, and reflective force rates may be easily modified without altering hardware. The location of the virtual pivot of the hand controller may be likewise readily changed.

EP 0 493 795 A1



Field of the Invention

The present invention pertains to hand controllers according to the preamble of claim 1 and particularly to aircraft hand controllers. More particularly, the invention pertains to displacement aircraft or space vehicle hand controllers.

Related Art

The related art involves conventional hand controllers which rotate about a fixed axis in the base, require movement of both the arm and the wrist, have a high force displacement gradient, and have either no or complex proprioceptive feedback.

In recent years, space and weight constraints in modern aircraft have resulted in compact fly-by-wire or fly-by-light control systems. Such systems reduce the size and weight of flight control hardware in the cockpit. In addition, these systems permit a side-arm controller configuration that reduces obstruction of the instrument panel area directly in front of the pilot. Two general configurations of those compact controllers have been developed—rigid and movable displacement. Rigid controllers measure the force of the control input and have no movement associated with input magnitude. Moveable controllers have a range of motion of about ± 5 cm (± 2 inches) to ± 10 cm (± 4 inches) associated with the magnitude of the control input. The force required to fully displace a moveable controller may be quite small, although the inclusion of a force-displacement gradient has been found to improve control performance.

Difficulties are associated with both types of hand controllers. Rigid controllers may produce severe operator fatigue due to a lack of proprioceptive feedback to tell the pilot how much force he is exerting. That difficulty can be reduced by allowing for a small (i.e., ± 6 mm or $\pm 1/4$ inch) amount of displacement or wobble unrelated to the force-output function. Further, rigid controllers provide fairly imprecise control and suffer from input axis cross-coupling, again due to the poor proprioceptive feedback provided to the operator.

Moveable controllers can provide reasonable control when a fairly heavy-force output gradient (i.e., ≥ 6.8 kg or $> \pm 15$ pounds at full displacement) is used; however, these force requirements result in operator fatigue. At lower force requirements, control imprecision and axis cross-coupling are resulting problems.

Some of these problems were solved upon the conception and development of a moveable hand controller configuration that permits accurate control while requiring a relatively low force-displacement gradient. Also, such hand controller is useful in a side-arm configuration in that it allows the operator's arm to remain essentially motionless in an arm rest while control inputs are made about the fulcrum of the wrist. When the operator provides an input, such hand controller assembly is rotated in an arc having its center at the operator's wrist and/or center is translational. The hand controller also has the advantage of rotation about the operator's wrist joint, thus requiring movement of the wrist only. In other words, that hand controller has a "virtual pivot" that permits inputs to be made about any point in space and the controller translates movement of the controller grip about a point in space (such as the operator's wrist joint) into movements of a sensor about an internal reference point thereby permitting one hand controller to optimally function for all hand sizes. However, that controller has a grip and a sensor platform with a small-displacement and a motion base with spring-loaded legs for flexibility. Such hand controller is disclosed in EP-A1-0 363 739.

Departing from this known hand controller, it is the object of the present invention to further improve it so that it can be matched to different applications. This object is achieved according to the characterizing features of claim 1. Further advantageous embodiments of the improved hand controller may be taken from the dependent claims.

Summary of the Invention

The present invention is still yet a further improvement on the related art. Not only does the present invention have a virtual pivot which accommodates variations in operator action, have six degrees of freedom, and variable pivot point locations; the invention is adaptable for providing various forces and torques and displacements and rotations and provides force feedback which simulates spring-type feedback but having different rates, various stop positions, variable damping, and a variety of reflective conditions to the controller environment including impact, proximity, limits, etc. The system of the invention has a hand controller incorporating system actuators, system sensors and feedback actuators which are connected to system control and force feedback control mechanisms which implement a variable control algorithm. The controller has a hand grip platform which is supported by telescoping legs. Linear actuators drive the

telescoping motion in the legs. Motors drive radial angular motion at the universal joints which attach the legs to the base plate. A force/torque sensor is attached to the hand grip platform and monitors control inputs from an operator of the hand controller. There are angular potentiometers, linear potentiometers, and motor tachometers associated with the telescoping legs. The potentiometers provide a measurement of the position and attitude of the platform with respect to the base. Signals from the force/torque sensor, angular potentiometers, linear potentiometers and motor tachometers are input into the control system. The control system sends signals to the motors to drive the hand controller to the commanded configuration with the appropriate force and feel characteristics at the hand grip.

The virtual pivot of the hand controller system accommodates a wide variety of operator sizes with a "floating" pivot point. Motors and controllers replace springs of the related art hand controller and yet provides force feedback or "feel". Spring rates, spring tension, damping rates, stop positions, the number of control axes, the dimensions and range of control axes, and force reflection characteristics may be programmed with various values based on specific requirements into the control system. The programmability and flexibility of the hand controller system permits the controlling of a large and varied range of devices with a single hand controller. The hand controller system may be programmed to compensate for various gravities, various gravity and inertial effects, or for gravity-free environments. Applications of the hand controller system include use in space stations, space vehicles, helicopters, fixed-wing aircraft, underwater vehicles, robotic vehicles, robotic arm controls, and other applications.

20 Brief Description of the Drawings

Figure 1 is a drawing of hand controller.

Figure 2 is an overview diagram of the hand controller, control system, and the controlled system.

Figure 3 is a graph showing the relationship of hand grip-applied force/torque versus hand controller movement displacement profiles.

Figure 4 illustrates the vector relationships between base and platform coordinate frames of the virtual pivot hand controller.

Figure 5a and 5b constitute a signal flow diagram of the control system and motor channels.

30 Description of the Preferred Embodiment

Figure 1 reveals an adaptable six degree of freedom virtual pivot hand controller 10. Virtual pivot hand controller 10 has a hand grip 28 for the operator's input. Hand grip 28 is connected through grip platform 30 to six degree of freedom force and torque sensor 34. Force and torque sensor 34 is an F/T series, model 75250 sensor from Assurance Technologies, Inc., of Garner, NC 27529. Grip platform 30 is connected to shafts 62 via ball joints 32. Three shafts 62 extend into three linear actuators 36, respectively. Linear actuators 36 cause shafts 62 to extend out of actuators 36 or to withdraw into actuators 36. The amount of shaft 62 extending out of linear actuator 36 is measured by linear potentiometer 38. Linear actuators 36 are driven by motors 40 thereby causing the extension or withdrawal of shafts 62. The withdrawal or extension of shafts 62 via ball joints 32 raise, lower, tilt, rotate and/or laterally move grip platform 30 and hand grip 28. The activity of motors 40 driving linear actuators 36 is monitored by tachometers 42. Linear actuators 36 are attached to universal joints 60, respectively. The other ends of the universal joints 60 opposite of linear actuators 36, are effectively attached to base plate 48. Six potentiometers 44 are, respectively, attached to universal joints 60 for measuring the angles of linear actuators 36 relative to base plate 48. The angle of linear actuator is 36, relative to base plate 48, is driven and set by motors 52 via gear heads 50 and worm and worm wheel assemblies 46. Gear heads 50 are attached to motors 52 through base plate 48 to worms 46. Worms 46 drive worm wheels 46 which are attached to the portions of universal joints 60 that are rigidly attached to linear actuators 36, respectively. Worms 46 driving worm wheels 46 set linear actuators 36 and shafts 62 to particular angles of inclination. Motors 52 are monitored by tachometers 54. Base plate 48 is supported by a surface 58 with structural supports 56. Surface 58 represents the place or area upon which hand controller 10 is situated and mounted.

Figure 2 reveals an overall diagram of the adaptable six degree of freedom virtual pivot hand controller 10 system. Hand controller 10 outputs sensor signals 20 from six degree of freedom force and torque sensor 34, linear potentiometers 38, angular potentiometers 44, motor tachometers 42 and motor tachometers 54. Sensor signals 20 are input to control system 12 which is a processor and specifically a Motorola VMEbus 68020 single board microcomputer, having system control 14 and force feedback control 16. Force and torque sensor 34 which is attached to hand grip platform and hand grip monitors the control inputs from the operator. Control system 12, in response to sensor signals 20, sends feedback signals to

motors 40 and 52 to drive hand controller 10 in accordance with the commanded configuration, having appropriate force and feel characteristics. The force and feel characteristics are determined by force feedback control 16 and response to sensor signals 20 revealing force, torque, position and rate, and signals from controlled system 18 sensors indicating proximity, force, field dynamics, etc., in response to driving signals 22 to system actuators such as motors, propulsion, etc. Hand controller 10 uses motor biasing to generate the force and feel of springs, damping and mechanical deadbands as illustrated in Figure 3. Figure 3 is a graph of hand grip applied force and torque versus displacement profiles of hand grip 10.

Control interface 22 required to determine hand control 10 orientation and translation in six degrees of freedom contains nine potentiometer measurements (three per leg) that define three position vectors of grip platform 10, corresponding to three fixed ball joints 32, with respect to the three base leg pivot points at the ends of shafts 62. During system calibration, a fixed displacement vector (from the origin of platform 30 coordinate frame) of the operator's wrist joint is estimated. Figure 4 shows the vector relationships between base 48 and platform 30 coordinate frames. Processor or control system 12, through force feedback control 18, returns three Euler angles and three linear translations from nominal platform 30 origin. Additionally, force and torque sensor 34 inputs are used in either position or rate mode to command a six degree of freedom velocity that motorized legs 36 and shaft drives 46 are to deliver. Thus, processor or control system 12 must first solve the geometric task of computing orientation and translation, and then compute the requisite leg or shaft rotational and linear velocities that result in the commanded and controller state.

Kinematic solutions to the hand grip platform Euler angles (defining attitude angles) and linear displacements from the center of the coordinate frame are obtained by use of nine potentiometers, 38 and 44. Fewer potentiometers can accomplish the same task of monitoring as the nine potentiometers. Telescoping legs or shafts 62 (whose links are actuator 36 driven) are attached to platform 30 by ball joints 32 and to base 48 by double-gimballed motorized joints 60. Outer gimbals 60 are rigidly attached to base 48, are motor 52 driven, and cause a roll motion about the leg or shaft 62 motor axis of rotation. Outer gimbal 62 axis defines the leg or shaft 62 coordinate frame X-axis for each of the three legs or shafts 62. These three axes are each oriented along the radial directions with respect to the center of base 48. This results in the forward base 48 point having its motor axes along the X-axis of the base 48 coordinate frame. Azimuth angles ϕ_i to the other two base 48 points have constant values of 120 and 240 degrees, respectively. Inner gimbals 60 allow rotation about the respective leg or shaft 62 pitch axes. Designating the length of the three legs 62 d_i , where i equals 1, 2, 3, and is defined $0 < d_{\min} < d_i < d_{\max}$. Then the position vectors of platform 30 ball joints 32 with respect to base 48 frame S_B :

$$\vec{P}_i = E_i(\Psi_0) E(\theta_i, \phi_i) \begin{bmatrix} 0 \\ 0 \\ d_i \end{bmatrix} + \vec{P}_{Bi}; \quad i = 1, 2, 3 \quad (1)$$

where

$$E(\theta_i, \phi_i) = \begin{bmatrix} \cos \theta_i & 0 & \sin \theta_i \\ \sin \theta_i \sin \phi_i & \cos \phi_i & -\cos \theta_i \sin \phi_i \\ -\sin \theta_i \sin \phi_i & \sin \phi_i & \cos \theta_i \cos \phi_i \end{bmatrix} \quad (2)$$

and

$$E_i(\psi_0) = \begin{bmatrix} \cos \psi_0 & -\sin \psi_0 & 0 \\ \sin \psi_0 & \cos \psi_0 & 0 \\ 0 & 0 & 1 \end{bmatrix}; \psi_0 = 0, 120, 240 \text{ deg} \\ \text{for } i = 1, 2, 3$$

(3)

Processor of control system 12 is a Motorola VMEbus 68020-board microcomputer housed in a standard Motorola chassis having several analog-to-digital interface cards. Six tachometers 42 and 54 on three legs 62 measure motor speeds of leg-extending or retracting motors 40 and leg-angular rotating motors 52. There are two motors, 40 and 52, per leg 62. Linear potentiometers 38 measure leg 62 extension and two angular potentiometers 44 per leg 62 measure angles of each leg 62 relative to base 48. There is a total of nine potentiometers 38 and 44.

Rate and position control modes of hand controller 10 differ. In the position mode, removal of grip, force and torque commands from the operator causes hand controller 10 to remain at its latest attained attitude and linear displacement. Removal of input in the rate mode will cause a return of hand controller 10 to the initial displacement origin. Any of the six degrees of freedom of hand controller 10 may be locked out as desired. Software stops are provided to prevent hand controller 10 from running into hard stops which might cause damage.

Figures 5a and 5b constitute an overview signal flow diagram of hand controller 10 input and motor control channels. This diagram has correlation with the program listing at the end of this description. Force/torque sensor 34 is a strain gauge type of sensor for detecting applied force and torque to hand grip 28 of controller 10. Interface 13 provides for keyboard or other type of input to the processor which includes input command processing 68 and motor command 70. Interface 13 is a RS-232 terminal interface for operator inputs of the controller 10 processor. Control system 66 provides for needed interaction among force and torque sensor 34, input command processing 68 and interface 13. Control system 66 includes sensor 34 electronics and control and may incorporate a Lord preprocessor and a Lord controller for sensor 34, from Assurance Technologies, Inc., of Garner, NC 27529. Controller function 72 incorporates software to perform the calculations of required motor rates to equal commanded input velocities of translation and rotation by incorporation kinematic system equations. Orientation function 74 incorporates software to perform the calculations of the platform and/or virtual pivot translation and rotation with respect to the base coordinate system. Inputs represent shaft or leg lengths, elevations and azimuth angles obtained from the nine potentiometers 38 and 44 (three per shaft or leg). Function 74 incorporates reverse kinematic system equations in its calculations. External object or device 18 receives input for external control and outputs signals for providing reflected force or torque (i.e., "feel" dynamics), or alarms.

The following describes the geometric relationships. Position vectors of the pivots are defined by \bar{R}_{Bi} and \bar{R}_{Pi} , where $i = 1, 2, 3$, in the two separate frames S_B (the base 48 frame) and S_P (the platform 30 frame), results in

$$\bar{R}_{B1} = \begin{bmatrix} r_B \\ 0 \\ 0 \end{bmatrix}; \bar{R}_{B2} = \begin{bmatrix} -r_B/2 \\ (\sqrt{3}/2)r_B \\ 0 \end{bmatrix}; \bar{R}_{B3} = \begin{bmatrix} -r_B/2 \\ -(\sqrt{3}/2)r_B \\ 0 \end{bmatrix}$$

$$R_{P1} = \begin{bmatrix} r_P \\ 0 \\ 0 \end{bmatrix}; R_{P2} = \begin{bmatrix} -r_P/2 \\ (\sqrt{3}/2)r_P \\ 0 \end{bmatrix}; R_{P3} = \begin{bmatrix} -r_P/2 \\ -(\sqrt{3}/2)r_P \\ 0 \end{bmatrix}$$

$$\bar{R}_C = \frac{1}{3} \sum_{i=1}^3 \left(\bar{R}_1 + \bar{R}_{Bi} \right) = \frac{1}{3} \sum_{i=1}^3 \bar{R}_1$$

since the sum $\sum \bar{R}_{Bi} = 0$.
or

$$\bar{R}_C = \frac{1}{3} \sum_{i=1}^3 E_i(\psi_0) \cdot \begin{bmatrix} -d_1 \sin \theta_1 \\ d_1 \cos \theta_1 \sin \phi_1 \\ -d_1 \cos \theta_1 \cos \phi_1 \end{bmatrix}$$

The above dot represents a matrix dot product. Referring to Figure 4, the platform $30 \hat{X}_P$ unit vector is directed from the center toward P_1 . The \hat{Y}_P unit vector is parallel to the line from P_3 to P_2 . Then,

$$\hat{X}_P = \left[\frac{1}{r_P} \right] \left[\bar{R}_1 - \bar{R}_C \right] = \left[\frac{2}{3} \bar{R}_1 - \frac{1}{3} (\bar{R}_2 + \bar{R}_3) \right]$$

$$\hat{Y}_P = \left[\frac{1}{\sqrt{3} r_P} \right] \left[\bar{R}_2 - \bar{R}_3 \right]$$

$$\hat{Z}_P = \hat{X}_P \times \hat{Y}_P = \left[\frac{2\sqrt{3}}{9r_P^2} \right] \left[\bar{R}_1 \times \bar{R}_2 + \bar{R}_2 \times \bar{R}_3 + \bar{R}_3 \times \bar{R}_1 \right]$$

The direction cosines of the \hat{X}_P , \hat{Y}_P , and \hat{Z}_P unit vectors are the components of the preceding vector equations. The Euler rotation matrix from S_0 to S_P is then

$$E_{P/B} = \begin{bmatrix} \hat{X}_P \cdot \hat{X}_B & \hat{Y}_P \cdot \hat{X}_B & \hat{Z}_P \cdot \hat{X}_B \\ \hat{X}_P \cdot \hat{Y}_B & \hat{Y}_P \cdot \hat{Y}_B & \hat{Z}_P \cdot \hat{Y}_B \\ \hat{X}_P \cdot \hat{Z}_B & \hat{Y}_P \cdot \hat{Z}_B & \hat{Z}_P \cdot \hat{Z}_B \end{bmatrix} = \left\{ e_{ij} \right\}.$$

The above dots represent vector dot products.

All information concerning the relative attitude orientation between the base 48 and platform 30 frames is contained in the Euler matrix $E_{P/B}$. Euler angles can be defined in 24 different ways depending on the sequence of rotations (in a positive sense about each of three axes). There are 12 permutations starting with either frame S_P or S_B , or 24 total. Each set of three angles is not interchangeable (except for very small rotations). Each set does, however, result in the same rotation of one frame to another when applied in its specific sequence.

The following set arises from a yaw rotation about the S_B z axis followed by a pitch rotation about the y axis and a final roll about the x axis:

$$\psi_P = \tan^{-1}(\theta_{12}/\theta_{11}) = \text{Yaw}$$

$$\theta_P = \sin^{-1}(\theta_{13}) = \text{Pitch}$$

$$\phi_P = \tan^{-1}(\theta_{23}/\theta_{33}) = \text{Roll}$$

Each rotation assumes the right-hand rule for positive sense. The inverse transformation performs a roll-pitch-yaw transformation (in that order) which is not uncommon in the aircraft industry.

The following describes the platform velocity equations. Tachometers 42 and 54 mounted on the handcontroller 10 legs and roll axis shafts are used in a velocity feedback controller 16 that drives each motorized leg 62 to null a separate commanded velocity. These six velocities are in turn computed according to the six signals from force/torque sensor 34 (after biasing to provide reflected force or torque dynamics for the operator).

At present, handgrip 28 force signals are interpreted as referenced to the base 48 coordinate frame as a linear velocity command. The coordinate system used is arbitrary and can be easily redefined in processor code and provided as an optional handcontroller 10 operating mode at a later time if desired.

The inertial velocity \vec{V}_i of each leg 62 is composed of the linear velocity of the platform 30 center summed with the rotational velocity about the center, that is

$$\vec{V}_i = \frac{d}{dt} \vec{R}_i = E_i(\psi_0) \left\{ \frac{d}{dt} \left[E_i(x_i, d_i) \cdot \begin{bmatrix} 0 \\ 0 \\ -d_i \end{bmatrix} \right] \right\}$$

$$= \vec{V}_C + \vec{\omega}_P (\vec{R}_i - \vec{R}_C); \quad i = 1, 2, 3$$

or

$$\vec{V}_i = n_i(\psi_0, \theta_i, \phi_i, d_i) \cdot \begin{bmatrix} \theta_i \\ \phi_i \\ d_i \end{bmatrix} = \vec{V}_C + \vec{\omega}_P (\vec{R}_i - \vec{R}_C);$$

$$i = 1, 2, 3$$

where $\dot{\theta}_i$, $\dot{\phi}_i$, and \dot{d}_i are the time rate of change of angles θ_i , ϕ_i , and leg length d_i for each leg. Then,

$$\begin{bmatrix} \dot{\theta}_i \\ \dot{\phi}_i \\ \dot{d}_i \end{bmatrix} = \Omega_i^{-1} [\vec{V}_C + \vec{\omega}_P (\vec{R}_i - \vec{R}_C)]; \quad i = 1, 2, 3$$

In the above equation, only the expressions for leg roll and length rates are of interest as the handcontroller 10 leg 62 pitching rates are automatically driven by mechanical constraints. This solution requires inversion of a 3 by 3 matrix, where

$$\Omega_i(\psi_0, \theta_i, \phi_i, d_i) = E_i(\psi_0) \cdot \begin{bmatrix} 0 & -d_i \cos\theta_i & -\sin\theta_i \\ d_i \cos\theta_i \cos\phi_i & -d_i \sin\theta_i \sin\phi_i & \cos\theta_i \sin\phi_i \\ d_i \cos\theta_i \sin\phi_i & d_i \sin\theta_i \cos\phi_i & -\cos\theta_i \cos\phi_i \end{bmatrix};$$

$$i = 1, 2, 3$$

The platform 30 angular velocity vector input commands, ω_P , above are referenced to S_0 ; if they are instead referenced to S_P , they are simply converted by the inverse Euler transformation as follows:

$$\omega_P = \begin{bmatrix} \omega_X \\ \omega_Y \\ \omega_Z \end{bmatrix}_B = E^{-1}_{P/B} \begin{bmatrix} \omega_X \\ \omega_Y \\ \omega_Z \end{bmatrix}_P$$

The inverse Euler matrix is the transpose of the matrix since the coordinate frame is orthogonal and Cartesian.

In summary, one feature of hand controller 10 is that the sensed location of the pivot point can be set arbitrarily. It can be set through the center of grip 28, above or below it, or be centered inside the operator's wrist. For example, with a pivot point below grip 28, it would act like a conventional military aircraft hand controller having the pivot point where the control stick attaches to the floor or deck of the aircraft. However, with the pivot point above grip 28, the top of the grip would be seemingly attached to a point above it and the grip would swing freely below it. The programmability of the pivot point provides for maximum flexibility and adaptability of hand controller 10. These changes in location of pivot point can be made by entering the appropriate software commands in control system 12. An initial setting can be made by the operator through the movement of his or her wrist for setting the virtual pivot and control swing and rotation dimensions in accordance with and to match the wrist movement. Other operating characteristics can be changed simply by altering the software. Such things as break out forces, the degree of freedom available, damping rates, spring tensions and velocity rates can be modified without altering the hardware of control system 12 or hand controller 10. Based on information from the vehicle or object being controlled, the

operator is given feedback through grip 28. This capability is force reflection and usually involves providing tactile feedback through grip 20 when the control object 18 (e.g., a robot arm or vehicle) contacts the target or other object. The combination of a programmable virtual pivot point having an active hand controller 10 allows the operator or user to configure hand controller 10 to match or meet the demands or needs of a particular task and user.

Motor-driven force feedback (microprocessor 12 control) replaces spring centering. Gradients of forces or torques versus displacements (in each of six axes), as shown in Figure 2, are stored as parameters that can be modified by keyboard 13 input. Such modification provides adaptability or programmability of key hand controller 10 operating characteristics including sensed (virtual) pivot axes locations and range of motion in each axis, sensed spring force reflection or the feel of grip 28 (i.e., force/displacement gradients), the capability, as desired, to implement bilateral force feedback from system 18 being controlled (via motor control feedback) to the human operator and the capability of operator-mode control to introduce menu-driven commands (via the VMEbus single-board computer).

APPENDIX

Software Listings for the Virtual Pivot Hand Controller

Filename	Description
handcntrbowl.c	Stand-alone test program for the "controller" function.
myfunc50hz.2.29.90	Main program (interrupt driven).
hc4.c	Merged "controller" and "orientation" functions.
hc4.h	Data structure definitions.
dtoa.h	Digital-to-analog conversions.
atod.h	Analog-to-digital conversions.
mymath.h	Sun Microsystems, Inc. utilities.
bowl.c	Bowl demonstration mode declarations.
cmd_declarations.h	Operator's terminal input commands.
cmd_definition.h	Data structure definitions.
makefile	Compiler macro command file.

Note: Additional file listings attached are minor utilities and data type definitions or declarations common to many similar implementations.

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/* .....Velocity Control Subroutine and Main Driver ..... */
/* Project: Virtual Pivot Hand Controller (IMD F4923-3000-2822) */
/*

/* Description: Theory of the C-Language code of this subprogram is
documented in the technical memo "Adaptable 6-DOF
Virtual Pivot Handcontroller: System Equations",
by W.C. Marshall, Dec 1989. Units are currently
inches, radians and seconds. Data I/O is via a data
structure as noted in the declarations.

Function "orient()" solves the "reverse kinematics"
problem given as input the desired platform's attitude
and relative position vector. Mean HEIGHT of the platform
specifies a positive distance along the "z" axis. The "g"
axis is positive down with the "z" axis away from the
operator and "y" axis toward the right.

Function "controller()" computes the linear and angular
velocities (inches & radians per second) of each leg and
shaft motor. Input are the relative linear and angular
velocity vectors of the platform center wrt the base.
Platform attitude and relative position vectors wrt the
platform origin (8.3" above base origin) are also output.

In the actual mechanism, function "orient()" is not
presently needed as "pots" measure the actual leg and
shaft displacements. Note that "zero" for the leg is when
the overall leg is at 9.5 inches and "zero" for shaft
rotation is when the leg is "vertical".

/* ..... Start of Global Declarations ..... */
#include <math.h>
#include <stdio.h>

```

```

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#define RPLAT 2.5
#define BRASE 2.5
#define HEIGHT 10.0
#define DCMOD 37.12577951
#define DCMOD 0.01743259
#define SRD2 .86602540
#define SRD3 .57735027
#define RPD2 RPLAT*.5
#define RPD2 BRASE*.5
#define HALF .5

/* Platform radius */
/* Base radius to leg */
/* Mean height of leg */
/* Degrees per radian */
/* Radians per degree */
/* Small number */
/* = sqrt(3)/2 */
/* = sqrt(3)/3 */
/* = (1/2)*RPLAT */
/* = (1/2)*BRASE */
/* = (1/2) */

/* Interface structure for "HandCtrl" I/O data */
/* Leg #1 length & two angles (Input) */
/* Leg #2 length & two angles (Input) */
/* Leg #3 length & two angles (Input) */
/* Current platform offset from zero position */
/* Current platform roll, pitch, yaw (radians) */
/* Desired translational rates */
/* Desired angular rates (rad./sec.) */
/* Angle & leg rate commands (Output) */
/* Angle & leg rate commands (Output) */
/* Angle & leg rate commands (Output) */

/* List of functions used by "main" */

void head();
void controller();
void orient();
void quat();
void euler();
void matmul();
void matran();
void transp();
void transpose();
void mmult();

/* MISCELLANEOUS */

static float gpb[3][3];
static float dmp[3][3];
static float elb[3][3];

/* Euler transformation matrix (Base-to-Platform) */
/* Euler transformation matrix (Platform-to-Base) */
/* Leg #1 euler matrix 8b to l1 */

```

```

static float e2b(3)(3);
static float e3b(3)(3);

static float e1(3)(3);
static float e2(3)(3);
static float e3(3)(3);
static float e1in(3)(3);
static float e2in(3)(3);
static float e3in(3)(3);

/* Leg #2 euler matrix Sb to L3
/* Leg #3 euler matrix Sb to L3

/* Leg #1 angular rate transform matrix
/* Leg #2 angular rate transform matrix
/* Leg #3 angular rate transform matrix
/* Inverse of #1 matrix
/* Inverse of #2 matrix
/* Inverse of #3 matrix

/* NEW PARAMETER LIST DECLARATIONS */

/* Euler angles phi,theta,pai wrt Sb
/* Platform rates Wx,Wy,Wz in Sb
/* Platform centerposition wrt Sb
/* Platform velocity wrt Sb
/* Position of Leg #1 at top in Sb
/* Position of Leg #2 at top in Sb
/* Position of Leg #3 at top in Sb
/* Velocity of Leg #1 at top in Sb
/* Velocity of Leg #2 at top in Sb
/* Velocity of Leg #3 at top in Sb
/* Real position of Leg #1 wrt R2(1)
/* Real position of Leg #2 wrt R2(1)
/* Real position of Leg #3 wrt R2(1)
/* Platform Sp unit vector coordinates
/* Platform Sp unit vector coordinates
/* Platform Sp unit vector coordinates
/* Motor rates for Leg #1
/* Motor rates for Leg #2
/* Motor rates for Leg #3

/* Commanded initial roll orientation
/* Commanded initial pitch orientation
/* Commanded initial yaw orientation
/* Platform position vector wrt Sb
/* Platform velocity wrt Sb
/* Computed Leg vectors in Sb
/* Computed Leg vectors in Sb at Bl
/* Computed Leg vectors in Sb at Bl
/* Computed Leg vectors in Sb at Bl
/* Computed Leg vectors in S1 at Bl
/* Computed euler matrix Sb to Sp
/* Constant matrix Sb to S1 for D1(3)

static float e2(3)(3) = (-HALF, GR3D2, 0, (-GR3D2,-HALF, 0), (1,0,1,0));

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static float ea3[3][3] = ((-HALF,-SK302,.0), ( SK302,-HALF,.0),(.0,.0,1.0));
/* Buffer for grip angular rate input */
static float pwa3[3];
/* Buffer for grip linear velocity input */
static float pvel[3];
/* Grip position offset vector */
static float gripos[3] = {1.0,.0,-3.13};
/* Grip vector in base coordinates */
static float gri[3];
/* Temporary vector storage */
static float daltax,daltay,daltaz;
/* Used in main program

static float dl,d2,d3;
static float thel,the2,the3;
static float phi1,phi2,phi3;
static float sthel,sth2,sth3;
static float sph1,sph2,sph3;
static float sphl,spbl,spbl2,spbl3;
static float sphl,spbl,spbl2,spbl3;
static float phi1,phi2,phi3d;
static float the1,the2,the3d;
static float dl,d2,d3d;
static float the1,the2,the3d;
static float phi1,phi2,phi3c;
static float phi1,phi2,phi3c;
static float the1,the2,the3c;

/* ..... BOWL DEMO DECLARATIONS ..... */
static float x,y,z; /* Bowl center coordinates above origin */
static float ALP = 78319816; /* 45 deg. from vertical in radians */
static float PID2 = 1.57079633; /* = (1/2)*pi radians or 90 deg. */
/* ..... */

void bowl(px,py,z,bowl,ybowl,xbowl,phibo,thebo,paibo)
float px,py;
float *bowl,*ybowl,*xbowl;
float *phibo,*thebo,*paibo;
float phi,the;

phi = PID2 - ALP*PX;
the = PID2 - ALP*PY;
*xbowl = RADIUS*cos(the)*cos(phi);
*ybowl = RADIUS*cos(the)*sin(phi);
*zbowl = RADIUS*sin(the) - RADIUS;
*phibo = PID2 - phi;
*thebo = PID2 - the;
*paibo = .0;

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return;
}

/* .....DEBUGGING DECLARATIONS..... */
static int BUG00 = 0; /* -1 means set I(-UNUSED-) */
static int BUG01 = 0; /* -1 means print eph[1][3] */
static int BUG02 = 0; /* -1 means print eph[1][4] */
static int BUG03 = 0; /* -1 means print R1,R2,R3 */
static int BUG04 = 0; /* -1 means print phi,d & did output */
static int BUG05 = 0; /* -1 means print vi,vectors */
static int BUG06 = 0; /* -1 means print euler angles commands */
static int BUG07 = 0; /* -1 means print euler angles results */
static int BUG08 = 0; /* -1 means print di,thai,phi */
static int BUG09 = 0; /* -1 means print euler matrix results */
static int BUG10 = 0; /* -1 means print di,thai,phi */
static int BUG11 = 0; /* -1 means print BVC[3] */
static int BUG12 = 0; /* -1 means print DA[3] */

/* ..... */
main()
{
    int j;

    float delta = .2;
    float x,y,z,th,phb,pab;
    float PX,PY;
    struct sensor sdata;
    j = 0;

    DELTA(0) = .0;
    DELTA(1) = .0;
    DELTA(2) = .0;
    PHIC = .1;
    THIC = .2;
    PSIC = -.3;

    orient(sdata);

    sdata.velx = .0;
    sdata.vely = .0;
    sdata.walt = 1.0;
    sdata.wx = .0;
    sdata.wy = .0;
    sdata.wz = 1.0;

    /* Set linear & angular velocities of the
       * sensor. Linear velocities defined
       * wrt SB with "x" down, "y" forward and
       * "z" axis towards the right. Angular
       *
       */

    /* Set vel. position & attitude of platform.
       * These variables are defined wrt SB.
       */

    /* Compute platform lag orientation
       *
       */

```

```

controller(sdata);
/* Compute motor velocity control */
deltax = sdata.deltax;
deltay = sdata.deltay;
deltaz = sdata.deltaz;
/* ..... Bowl Demo Test ..... */
PX = -1.;
PY = -1.;
for(j=0;j<10;j++)
{
    PX = PX + deltax;
    PY = PY + deltay;
    bowl(PX,PY,sab,syb,spab,spbb,spcb,spcb);
    printf("PX,PY = %2.3f %2.3f \n", PX,PY);
    printf("Pxb,Pyb,spxb,spyb = %2.3f %2.3f %2.3f %2.3f \n", pxb,pyb,spxb,spyb);
}

/* DEBUG LOGIC CONTROL */
if(hu001>0) printf(" 01:epb[0][5] = %2.3f %2.3f %2.3f \n",epb[0][0],epb[0][1],epb[0][2]);
if(hu001>0) printf(" 01:epb[1][5] = %2.3f %2.3f %2.3f \n",epb[1][0],epb[1][1],epb[1][2]);
if(hu001>0) printf(" 01:epb[2][5] = %2.3f %2.3f %2.3f \n",epb[2][0],epb[2][1],epb[2][2]);
if(hu001>0) printf(" 01:epb[3][5] = %2.3f %2.3f %2.3f \n",epb[3][0],epb[3][1],epb[3][2]);
if(hu001>0) printf(" 01:epb[4][5] = %2.3f %2.3f %2.3f \n",epb[4][0],epb[4][1],epb[4][2]);
if(hu001>0) printf(" 01:epb[5][5] = %2.3f %2.3f %2.3f \n",epb[5][0],epb[5][1],epb[5][2]);
if(hu001>0) printf(" 01:al,a2,a3,ap,a2,3f %2.3f %2.3f %2.3f \n",al[0],a2[0],a3[0],ap[0]);
if(hu001>0) printf(" 01:a1,a2,a3,ap,a2,3f %2.3f %2.3f %2.3f \n",a1[0],a2[0],a3[0],ap[0]);
if(hu001>0) printf(" 01:phid,a2,3f %2.3f %2.3f %2.3f \n",phid,a2,a3);
if(hu001>0) printf(" 01:did %2.3f %2.3f %2.3f \n",did,d2a,d3a);
if(hu001>0) printf(" 01:vi-a2,3f %2.3f %2.3f %2.3f \n",vi[0],vi[1],vi[2]);
if(hu001>0) printf(" 01:vi-a2,3f %2.3f %2.3f %2.3f \n",vi[0],vi[1],vi[2]);
if(hu001>0) printf(" 01:phic,the,pa2,3f %2.3f %2.3f %2.3f \n",phic,the,pa2);
if(hu001>0) printf(" 01:PHIC,the,pa2,3f %2.3f %2.3f %2.3f \n",PHIC,the,pa2);
if(hu001>0) printf(" 01:epb[0][5] = %2.3f %2.3f %2.3f \n",epb[0][0],epb[0][1],epb[0][2]);
if(hu001>0) printf(" 01:epb[1][5] = %2.3f %2.3f %2.3f \n",epb[1][0],epb[1][1],epb[1][2]);
if(hu001>0) printf(" 01:epb[2][5] = %2.3f %2.3f %2.3f \n",epb[2][0],epb[2][1],epb[2][2]);
if(hu001>0) printf(" 01:thec %2.3f %2.3f %2.3f \n",thec,the,thec);
if(hu001>0) printf(" 01:dic %2.3f %2.3f %2.3f \n",dic,d2c,d3c);
if(hu001>0) printf(" 01:phi1,phi2,phi3 %2.3f %2.3f %2.3f \n",phi1,phi2,phi3);

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    D3b[0] = R3b[0] + HALF*BASE;
    D3b[1] = R3b[1] + SHD2*BASE;
    D3b[2] = R3b[2];

    d1c2 = .0;
    for(j=0;j<3;j++) d1c2 = d1c2 + D1b[j]*D1b[j];
    for(i=0;i<3;i++) d2c2 = d2c2 + D2b[j]*D2b[j];
    d3c2 = .0;
    for(j=0;j<3;j++) d3c2 = d3c2 + D3b[j]*D3b[j];

    for(j=0;j<3;j++) L21[j] = D1b[j];

    matcopy (&t2,D2b,L22);
    matcopy (&t3,D3b,L23);

    d1c = sqrt(d1c2);
    d2c = sqrt(d2c2);
    d3c = sqrt(d3c2);

    phi1c = atan2(L21[1],d1c);
    theta1 = asin(-L21[0]/sqrt(L21[0]*L21[0] + L21[2]*L21[2]));
    phi2c = atan2(L22[1],d2c);
    theta2 = asin(-L22[0]/sqrt(L22[0]*L22[0] + L22[2]*L22[2]));
    phi3c = atan2(L23[1],d3c);
    theta3 = asin(-L23[0]/sqrt(L23[0]*L23[0] + L23[2]*L23[2]));

    /* ..... */
    /* Set output values */
    sdata->d1 = d1c;
    sdata->d1c1 = theta1;
    sdata->phi1 = phi1c;
    sdata->d2 = d2c;
    sdata->phi2 = phi2c;
    sdata->d3 = d3c;
    sdata->theta3 = theta3c;
    sdata->phi3 = phi3c;

    return;

```

```

/* .....End of orient function.....*/
/* .....Start of Velocity Control Function .....*/

void controller(sdata)
struct sensor *sdata;
{
    int i;
    float det1,det2,det3;

    d1 = sdata->d1;
    the1 = sdata->the1;
    phi1 = sdata->phi1;
    d2 = sdata->d2;
    the2 = sdata->the2;
    phi2 = sdata->phi2;
    d3 = sdata->d3;
    the3 = sdata->the3;
    phi3 = sdata->phi3;

    VEL[0] = sdata->velx;
    VEL[1] = sdata->vely;
    VEL[2] = sdata->velz;
    pracc[0] = sdata->wex;
    pracc[1] = sdata->wey;
    pracc[2] = sdata->wez;

    athe1 = sin(the1);
    cthe1 = cos(the1);
    aph1 = sin(phi1);
    ophi1 = cos(phi1);
    athe2 = sin(the2);
    cthe2 = cos(the2);
    aph2 = sin(phi2);
    ophi2 = cos(phi2);
    athe3 = sin(the3);
    cthe3 = cos(the3);
    aph3 = sin(phi3);
    ophi3 = cos(phi3);

    /* Transfer input data from global storage */

    /* Get desired linear & angular velocities
       * Input is assumed to be in 3d coord. */
    /* Input is assumed to be in 3d coord. */
    /* Compute sines & cosines */
}

```

```

/* Compute R1,R2,R3,RP vectors */
R1[0] = -d1*etha1 + RBASE;
R1[1] = -d1*etha1*eph11;
R1[2] = -d1*etha1*eph11;
R2[0] = d2*(HALF*etha2) - (SRD2*etha2*eph12)) - RD02;
R2[1] = d2*((SRD2*etha2) - (HALF*etha2*eph12)) + SRD2*RBASE;
R2[2] = -d2*etha2*eph12;
R3[0] = d3*(HALF*etha3) * ( SRD2*etha3*eph13) - RD02;
R3[1] = d3*((SRD2*etha3) - (HALF*etha3*eph13)) - SRD2*RBASE;
R3[2] = -d3*etha3*eph13;
/* Compute Platform origin position vector*/
for(j=0; j<3; j++) RP[j] = (1.0/3.0)*(R1[j] + R2[j] + R3[j]);

/* Compute euler matrix epb(t1,t) */
for(j=0; j<3; j++) XP[j] = R1[j] - RP[j]/RPAT;
for(j=0; j<3; j++) YP[j] = R2[j] - RP[j]/RPAT;
for(j=0; j<3; j++) ZP[j] = R3[j] - RP[j]/RPAT;
XP[0] = XP[1]*YP[2] - (ZP[0]*YP[2]);
XP[1] = (XP[2]*YP[0]) - (ZP[0]*YP[2]);
YP[2] = (XP[0]*YP[1]) - (ZP[1]*YP[0]);
for(j=0; j<3; j++) epb[0][j] = XP[j];
for(j=0; j<3; j++) epb[1][j] = YP[j];
for(j=0; j<3; j++) epb[2][j] = ZP[j];

transpose(epb,ebp);
matcopy(epb,prts,ANATE);

/* Obtain euler matrix ebp(t1,t) */
/* Convert prts(t1) to Sb coord. */
/* Compute Leg position wrt Sp in Sb */
for(j=0; j<3; j++) RP1[j] = R1[j] - RP[j];
for(j=0; j<3; j++) RP2[j] = R2[j] - RP[j];
for(j=0; j<3; j++) RP3[j] = R3[j] - RP[j];
/* Compute linear velocity of legs */
V1[0] = VEL[0] + (ARATE[1]*RP1[2] - ANATE[2]*RP1[1]);
V1[1] = VEL[1] + (ARATE[2]*RP1[0] - ANATE[0]*RP1[2]);
V1[2] = VEL[2] + (ARATE[0]*RP1[1] - ANATE[1]*RP1[0]);
V2[0] = VEL[0] + (ARATE[1]*RP2[2] - ANATE[2]*RP2[1]);
V2[1] = VEL[1] + (ARATE[2]*RP2[0] - ANATE[0]*RP2[2]);
V2[2] = VEL[2] + (ARATE[0]*RP2[1] - ANATE[1]*RP2[0]);
V3[0] = VEL[0] + (ARATE[1]*RP3[2] - ANATE[2]*RP3[1]);
V3[1] = VEL[1] + (ARATE[2]*RP3[0] - ANATE[0]*RP3[2]);
V3[2] = VEL[2] + (ARATE[0]*RP3[1] - ANATE[1]*RP3[0]);

```

```

/* Compute rate transform matrices */

a1[0][0] = .0;
a1[1][0] = d1*ctha1*cpb1;
a1[2][0] = d1*ctha2*cpb1;
a1[0][1] = -d1*ctha1;
a1[1][1] = -d1*ctha1*spb1;
a1[2][1] = -d1*ctha1*cpb1;
a1[0][2] = -ctha1;
a1[1][2] = -ctha1*spb1;
a1[2][2] = -ctha1*cpb1;

e2[0][0] = d2*(-s3d2*ctha2*cpb12);
e2[1][0] = d2*(-HALF*ctha2*cpb12);
e2[2][0] = d2*ctha2*cpb12;
e2[0][1] = d3*(-HALF*ctha2);
e2[1][1] = d3*(-s3d2*ctha2 + (HALF*ctha2*spb12));
e2[2][1] = d3*ctha2*cpb12;
e2[0][2] = ((HALF*ctha3) - (s3d2*ctha3*cpb13));
e2[1][2] = ((-s3d2*ctha3) - (HALF*ctha3*spb13));
e2[2][2] = -ctha3*cpb13;

e3[0][0] = d3*(s3d2*ctha3*cpb13);
e3[1][0] = d3*(-HALF*ctha3*cpb13);
e3[2][0] = d3*ctha3*cpb13;
e3[0][1] = d3*(HALF*ctha3) + (s3d2*ctha3*spb13);
e3[1][1] = d3*(-s3d2*ctha3 + (HALF*ctha2*cpb13));
e3[2][1] = d3*ctha3*cpb13;
e3[0][2] = ((HALF*ctha3) + (s3d2*ctha3*spb13));
e3[1][2] = ((s3d2*ctha3) - (HALF*ctha3*cpb13));
e3[2][2] = -ctha3*cpb13;

/* Form final matrices */

matinv(e1,e1n,fdet1);
matinv(e2,e2n,fdet2);
matinv(e3,e3n,fdet3);

matmul(e1n,v1,dv1);
matmul(e2n,v2,dv2);
matmul(e3n,v3,dv3);

phd = OUT1(0);
ph2 = OUT2(0);
ph3 = OUT3(0);
did = OUT1(2);
dtd = OUT2(2);
dd = OUT3(2);

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/* Compute ONE SET of euler angles (of 121)
*/

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/* This set is psi, theta, phi (in order) 8b to 3p */
*/

ANGLE[0] = atan2(epb[1][2], epb[2][2]);
ANGLE[1] = asin(-epb[0][2]);
ANGLE[2] = atan2(epb[0][1], epb[0][0]);

/* ..... */

/* Transfer Output Data */

sdota->phidot = phld;
sdota->phidot = phld;
sdota->phidot = phld;

sdota->didot = did;
sdota->ddidot = ddd;
sdota->ddidot = ddd;

matcopy(epb, griploc, grip);

sdota->delx = RF[0] * grip[0];
sdota->dely = RF[1] * grip[1];
sdota->delz = RF[2] * HEIGHT + grip[2];

sdota->phi = ANGLE[0];
sdota->theta = ANGLE[1];
sdota->psi = ANGLE[2];

return;
}

/* ..... End of Velocity Control Pn. .... */

void quat(q1, q2, q3, q4, trans)
float q1, q2, q3, q4;
float trans[3][3];
{
    /* Compute new transformation matrix */

    trans[0][0] = (q1*q1 + q2*q2 + q3*q3 + q4*q4);
    trans[0][1] = 2*(q1*q2 - q3*q4);
    trans[0][2] = 2*(q2*q3 + q1*q4);
    trans[1][0] = 2*(q2*q3 - q1*q4);
    trans[1][1] = (q1*q1 - q2*q2 + q3*q3 - q4*q4);
    trans[1][2] = 2*(q3*q4 + q1*q2);
    trans[2][0] = 2*(q3*q4 - q1*q2);
    trans[2][1] = 2*(q3*q4 - q1*q2);
    trans[2][2] = (q1*q1 - q2*q2 - q3*q3 + q4*q4);
}

```

```

return;
}
/* ..... */
void euler(phi,the,psi,mat)
float phi,the,psi;
float mat[3][3];
{
    float sphi,cphi,scthe,cthe,spai,cpai;
    /* ..... Euler Matrix Computation ..... */
    /* Compute euler rotation matrix from 100-Vect. to Body */
    scthe = sin(the);
    ccthe = cos(the);
    spai = sin(pai);
    cpai = cos(pai);
    sphi = sin(phi);
    cphi = cos(phi);
    mat[0][0] = ccthe*cpai;
    mat[0][1] = ccthe*spai;
    mat[0][2] = ccthe;
    mat[1][0] = sphi*scthe*cpai - cphi*spai;
    mat[1][1] = sphi*scthe*spai + cphi*cpai;
    mat[1][2] = sphi*ccthe;
    mat[2][0] = cphi*scthe*cpai + sphi*cpai;
    mat[2][1] = cphi*scthe*spai - sphi*cpai;
    mat[2][2] = cphi*ccthe;
    return;
}
/* ..... */
void matcopy(a,b,c)
/* Matrix(3x3) times vector (1x3) */
/* Calling sequence:
   float m[3][3];
   float v[3];
   matcopy(m,v,v)
*/
float a[3][3];

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float b[3] ;
float c[3] ;

{
    float t[3] ;
    t[0] = a[0][0]*b[0] + a[0][1]*b[1] + a[0][2]*b[2] ;
    t[1] = a[1][0]*b[0] + a[1][1]*b[1] + a[1][2]*b[2] ;
    t[2] = a[2][0]*b[0] + a[2][1]*b[1] + a[2][2]*b[2] ;
    c[0] = t[0] ;
    c[1] = t[1] ;
    c[2] = t[2] ;
}

/* ..... End "matmty" Code ..... */

void matran(a,b,c)
/* Matrix transposition multiply */
/* Matrix a is a square vector (n,n) */
/* Calling sequence: */
/* float m3[3] ; */
/* float v[3] ; */
/* matran(m,v,v) */
{
    float a[3][3] ;
    float b[3] ;
    float c[3] ;

    float t[3] ;
    t[0] = a[0][0]*b[0] + a[1][0]*b[1] + a[2][0]*b[2] ;
    t[1] = a[0][1]*b[0] + a[1][1]*b[1] + a[2][1]*b[2] ;
    t[2] = a[0][2]*b[0] + a[1][2]*b[1] + a[2][2]*b[2] ;
    c[0] = t[0] ;
    c[1] = t[1] ;
    c[2] = t[2] ;
}

/* ..... End "matran" Code ..... */

void matinv(a,b,det)
/* Matrix (3x3) Inverse & Determinant) */
/* Calling sequence: */
/* float m3[3] ; */
/* float n3[3] ; */
/* float *det */

```



```

/* matinv(m,n,det) */
/* Cramer's Rule used to compute inverse.
/* Inverse of m to n (with determinant returned always)
/* If det "smaller" than "tiny", inverse not returned */
*/

float a[3][3] ;
float b[3][3] ;
float det ;

{
    *det = a[0][0] * (a[1][1]*a[2][2] - a[1][2]*a[2][1])
          + a[1][0] * (a[2][1]*a[0][2] - a[0][1]*a[2][2])
          + a[2][0] * (a[0][1]*a[1][2] - a[1][1]*a[0][2]);
    if (fabs(*det)<TINY) return;
    temp = 1.0/(*det);
    b[0][0] = temp * (a[1][1]*a[2][2] - a[1][2]*a[2][1]);
    b[1][0] = -temp * (a[1][0]*a[2][2] - a[1][2]*a[2][0]);
    b[2][0] = temp * (a[1][0]*a[2][1] - a[1][1]*a[2][0]);
    b[0][1] = -temp * (a[0][1]*a[2][2] - a[0][2]*a[2][1]);
    b[1][1] = temp * (a[0][0]*a[2][2] - a[0][2]*a[2][0]);
    b[2][1] = -temp * (a[0][0]*a[2][1] - a[0][1]*a[2][0]);
    b[0][2] = temp * (a[0][1]*a[1][2] - a[0][2]*a[1][1]);
    b[1][2] = -temp * (a[0][0]*a[1][2] - a[0][2]*a[1][0]);
    b[2][2] = temp * (a[0][0]*a[1][1] - a[0][1]*a[1][0]);
}

/* ..... End "matinv" Code ..... */

void mmult(a,b,c)
/* Matrix(3x3) times matrix(3x3) */
/* Calling sequence:
/* float a[3][3] ;
/* float b[3][3] ;
/* float c[3][3] ;
/* mmult(a,b,c) ;
/* (a[i][b] -> c)
*/

float a[3][3] ;
float b[3][3] ;
float c[3][3] ;
{
    c[0][0] = a[0][0]*b[0][0] + a[0][1]*b[1][0] + a[0][2]*b[2][0] ;

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c[1][0] = a[1][0]*b[0][0] + a[1][1]*b[1][0] + a[1][2]*b[2][0] /
c[2][0] = a[2][0]*b[0][0] + a[2][1]*b[1][0] + a[2][2]*b[2][0] /

c[0][1] = a[0][0]*b[0][1] + a[0][1]*b[1][1] + a[0][2]*b[2][1] /
c[1][1] = a[1][0]*b[0][1] + a[1][1]*b[1][1] + a[1][2]*b[2][1] /
c[2][1] = a[2][0]*b[0][1] + a[2][1]*b[1][1] + a[2][2]*b[2][1] /

c[0][2] = a[0][0]*b[0][2] + a[0][1]*b[1][2] + a[0][2]*b[2][2] /
c[1][2] = a[1][0]*b[0][2] + a[1][1]*b[1][2] + a[1][2]*b[2][2] /
c[2][2] = a[2][0]*b[0][2] + a[2][1]*b[1][2] + a[2][2]*b[2][2] /
}

/* ..... End "mult" Code ..... */

void transpose(a,b)
/* Matrix[3x3] transpose to matrix[3x3] */
/* Calling sequence:
/* float a[3][3] /
/* float b[3][3] /
/* transpose(a,b) /
/* (a)' -> (b) */

float a[3][3] /
float b[3][3] /

b[0][0] = a[0][0] /
b[1][0] = a[0][1] /
b[2][0] = a[0][2] /
b[0][1] = a[1][0] /
b[1][1] = a[1][1] /
b[2][1] = a[1][2] /
b[0][2] = a[2][0] /
b[1][2] = a[2][1] /
b[2][2] = a[2][2] /
}

/* ..... End "mult" Code ..... */

```

```

#include "../include/mem_map.h"
#include "../include/dtoa.h"
#include "../include/hci.h"

#define extern
#include "../include/vp.h"
#undef extern

#define DOIP asm("    bset    $t5,$f0f00001");
    unsigned long card(3);
    double lim();
    struct sensor ho;
    double phic,thae,palo,xo,yo,sc,px,py;
/*-----*/
myfunc50hz()
{
    static int k25 = 0;
    static int k10 = 2;
    static int k02 = 2;
    static int k01 = 4;

    /* asm("    bset    $t5,$f0f00001"); */
    asm("    bset    $t5,$f0f00001");

    k25 = (k25 + 1) % 2;
    k10 = (k10 + 1) % 5;
    k05 = (k05 + 1) % 10;
    k02 = (k02 + 1) % 25;
    k01 = (k01 + 1) % 50;

    do50hz();

    if (k25 == 0)
    {
        |
    }

    if (k10 == 0)
    {
        |
    }

    if (k05 == 0)
    {
        |
    }
}

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if (a02 == 0)
{
}

if (a01 == 0)
{
}

/* am(" bolz 485,99990001"), */
}

/*-----*/
intmyfunc5hr1()
{
vp.igo = INT_OFF;
vp.mod = POS_MODE;
vp.csr = INT_OFF;
vp.scl = POSL_OFF;
vp.hp = 1.0;
vp.hr = 15.0;

MAX_FORCE = 15.0;
MAX_MOMENT = 200.0;

/* initialize fcs, ioo, atod, and dtoa */
vls_init(ERM_ADRN);
atod_init(EO_LEVEL,VME_LEVEL,VECTOR);
dtoa_init();

card[0] = dtoa_define(A_BASE_ADRN,1,RANGE);
card[1] = dtoa_define(C_BASE_ADRN,1,RANGE);
card[2] = atod_define(C_BASE_ADRN,C_RANGE,C_CHANNELS);

/* assign channels and cards for pots and tachs */

leg1.lin.rat.chn = 0; leg1.lin.rat.crd = 2;
leg1.lin.pos.chn = 1; leg1.lin.pos.crd = 2;
leg1.rad.pos.chn = 2; leg1.rad.pos.crd = 2;
leg1.tan.rat.chn = 3; leg1.tan.rat.crd = 2;
leg1.tan.pos.chn = 4; leg1.tan.pos.crd = 2;
leg2.lin.rat.chn = 5; leg2.lin.rat.crd = 2;
leg2.lin.pos.chn = 6; leg2.lin.pos.crd = 2;
leg2.rad.pos.chn = 7; leg2.rad.pos.crd = 2;
leg2.tan.rat.chn = 8; leg2.tan.rat.crd = 2;
leg2.tan.pos.chn = 9; leg2.tan.pos.crd = 2;

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```

leg3.lin.set.chn = 10; leg3.lin.set.ord = 2;
leg3.lin.pos.chn = 11; leg3.lin.pos.ord = 2;
leg3.rad.set.chn = 12; leg3.rad.set.ord = 2;
leg3.tan.set.chn = 13; leg3.tan.set.ord = 2;
leg3.tan.pos.chn = 14; leg3.tan.pos.ord = 2;

/* assign channels and cards for motor drivers */
leg1.lin.mot.chn = 1; leg1.lin.mot.ord = 0;
leg1.tan.mot.chn = 2; leg1.tan.mot.ord = 0;
leg2.lin.mot.chn = 3; leg2.lin.mot.ord = 0;
leg2.tan.mot.chn = 4; leg2.tan.mot.ord = 0;
leg3.lin.mot.chn = 1; leg3.lin.mot.ord = 1;
leg3.tan.mot.chn = 2; leg3.tan.mot.ord = 1;

/* zero integrators for rate and position loops */
leg1.lin.set.ier = 0.0;
leg1.tan.set.ier = 0.0;
leg2.lin.set.ier = 0.0;
leg2.tan.set.ier = 0.0;
leg3.lin.set.ier = 0.0;
leg3.tan.set.ier = 0.0;

/* set motor driver outputs to 0.0v */
dtoa_write(card[leg1.lin.mot.ord], leg1.lin.mot.chn, VOLTAGE, 0.0);
dtoa_write(card[leg1.tan.mot.ord], leg1.tan.mot.chn, VOLTAGE, 0.0);
dtoa_write(card[leg2.lin.mot.ord], leg2.lin.mot.chn, VOLTAGE, 0.0);
dtoa_write(card[leg2.tan.mot.ord], leg2.tan.mot.chn, VOLTAGE, 0.0);
dtoa_write(card[leg3.lin.mot.ord], leg3.lin.mot.chn, VOLTAGE, 0.0);
dtoa_write(card[leg3.tan.mot.ord], leg3.tan.mot.chn, VOLTAGE, 0.0);
}

/* ===== */
double limit, min, max;
double x, minf, maxf;
{
    if (x < min) return(min);
    if (x > max) return(max);
}

```

```

return (a);
}

/*-----*/
des5shr(t)
{
    etcod_read(card[leg1.lin.ret.crd], leg1.lin.ret.chin, &dc0, &leg1.lin.ret.val);
    etcod_read(card[leg1.lin.ret.crd], leg1.lin.ret.chin, &dc0, &leg1.lin.ret.val);
    etcod_read(card[leg1.lin.ret.crd], leg1.lin.ret.chin, &dc0, &leg1.lin.ret.val);
    etcod_read(card[leg1.ten.crd], leg1.ten.ret.chin, &dc0, &leg1.ten.ret.val);
    etcod_read(card[leg1.ten.crd], leg1.ten.ret.chin, &dc0, &leg1.ten.ret.val);
    etcod_read(card[leg1.ten.crd], leg1.ten.ret.chin, &dc0, &leg1.ten.ret.val);
    etcod_read(card[leg1.red.pos.crd], leg1.red.pos.chin, &dc0, &leg1.red.pos.val);
    etcod_read(card[leg1.red.pos.crd], leg1.red.pos.chin, &dc0, &leg1.red.pos.val);
    etcod_read(card[leg2.lin.ret.crd], leg2.lin.ret.chin, &dc0, &leg2.lin.ret.val);
    etcod_read(card[leg2.lin.ret.crd], leg2.lin.ret.chin, &dc0, &leg2.lin.ret.val);
    etcod_read(card[leg2.ten.crd], leg2.ten.ret.chin, &dc0, &leg2.ten.ret.val);
    etcod_read(card[leg2.ten.crd], leg2.ten.ret.chin, &dc0, &leg2.ten.ret.val);
    etcod_read(card[leg2.ten.crd], leg2.ten.ret.chin, &dc0, &leg2.ten.ret.val);
    etcod_read(card[leg2.red.pos.crd], leg2.red.pos.chin, &dc0, &leg2.red.pos.val);
    etcod_read(card[leg2.red.pos.crd], leg2.red.pos.chin, &dc0, &leg2.red.pos.val);
    etcod_read(card[leg3.lin.ret.crd], leg3.lin.ret.chin, &dc0, &leg3.lin.ret.val);
    etcod_read(card[leg3.lin.ret.crd], leg3.lin.ret.chin, &dc0, &leg3.lin.ret.val);
    etcod_read(card[leg3.ten.crd], leg3.ten.ret.chin, &dc0, &leg3.ten.ret.val);
    etcod_read(card[leg3.ten.crd], leg3.ten.ret.chin, &dc0, &leg3.ten.ret.val);
    etcod_read(card[leg3.ten.crd], leg3.ten.ret.chin, &dc0, &leg3.ten.ret.val);
    etcod_read(card[leg3.red.pos.crd], leg3.red.pos.chin, &dc0, &leg3.red.pos.val);
    etcod_read(card[leg3.red.pos.crd], leg3.red.pos.chin, &dc0, &leg3.red.pos.val);

    /* convert tangential mass. to rad and sec, right hand rule, thumb out */
    hc.ph11 = leg1.ten.pos.val*TM_Pos_SF;
    hc.ph12 = leg2.ten.pos.val*TM_Pos_SF;
    hc.ph13 = leg3.ten.pos.val*TM_Pos_SF;

    /* convert radial mass. to rad and sec, positive leg top in */
    hc.th11 = -leg1.red.pos.val*RD_Pos_SF;
    hc.th12 = -leg2.red.pos.val*RD_Pos_SF;
    hc.th13 = -leg3.red.pos.val*RD_Pos_SF;

    /* convert linear mass. to inches, positive leg extended */
    hc.d1 = -leg1.lin.pos.val*LIN_Pos_SF + LIN_Pos_OFF;
    hc.d2 = -leg2.lin.pos.val*LIN_Pos_SF + LIN_Pos_OFF;
    hc.d3 = -leg3.lin.pos.val*LIN_Pos_SF + LIN_Pos_OFF;

    /* convert linear techs to positive leg extending */
    leg1.lin.ret.val = -leg1.lin.ret.val;
    leg2.lin.ret.val = -leg2.lin.ret.val;
    leg3.lin.ret.val = -leg3.lin.ret.val;

```

```

/* controller */
hc.velx = 0.0;
hc.vely = 0.0;
hc.velz = 0.0;
hc.wx = 0.0;
hc.wy = 0.0;
hc.ws = 0.0;
if (vp.boi == BOWL_ON)
{
    pz = -lim(vp.mz/MAX_MOMENT,-1.0,1.0);
    py = -lim(vp.mx/MAX_MOMENT,-1.0,1.0);
    bow(pz,py,psc,pyo,psc,phic,thetac,epsio);
    hc.velx = vp.kp*(sc - hc.dels);
    hc.vely = vp.kp*(yc - hc.dely);
    hc.velz = vp.kp*(sc - (lim_pos_off + hc.dels));
    hc.wx = vp.kp*(phic - hc.phi);
    hc.wy = vp.kp*(thetac - hc.theta);
    hc.ws = vp.kp*(psio - hc.psi);
}
if (vp.boi == BOWL_OFF)
{
    if (vp.mod == RATE_MODE)
    {
        xc = 0.0;
        yc = 0.0;
        pc = 0.0;
        if (vp.dof == SIX_DOF)
        {
            xc = lim(vp.fx/MAX_FORCE,-MAX_TRANS_MAX_TRANS);
            yc = lim(vp.fy/MAX_FORCE,-MAX_TRANS_MAX_TRANS);
            pc = lim(vp.fz/MAX_FORCE,-MAX_TRANS_MAX_TRANS);
        }
        hc.velx = vp.kp*(sc - hc.dels);
        hc.vely = vp.kp*(yc - hc.dely);
        hc.velz = vp.kp*(sc - (lim_pos_off + hc.dels));
        phic = lim(vp.mz/MAX_MOMENT,-MAX_ANGLE_MAX_ANGLE);
        thetac = lim(vp.mx/MAX_MOMENT,-MAX_ANGLE_MAX_ANGLE);
        psio = lim(vp.mz/MAX_MOMENT,-MAX_ANGLE_MAX_ANGLE);
        hc.wx = vp.kp*(phic - hc.phi);
    }
}

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    hc.vy = vp.kp*(ctao - hc.theta);
    hc.vx = vp.kp*(pao - hc.pai);
  }
  if (vp.mod == POS_MODE)
  {
    if (vp.dof == SIX_DOF)
    {
      if (vp.fy > FORCE_BAND) hc.velx = 1.0;
      if (vp.fy < -FORCE_BAND) hc.velx = -1.0;
      if (vp.fx > FORCE_BAND) hc.vely = 1.0;
      if (vp.fx < -FORCE_BAND) hc.vely = -1.0;
      if (vp.fs > FORCE_BAND) hc.velz = 0.3;
      if (vp.fs < -FORCE_BAND) hc.velz = -0.3;
      if (vp.fz > FORCE_BAND) hc.velx = 0.3;
      if (vp.fz < -FORCE_BAND) hc.velx = -0.3;
      if (vp.mz > MOM_BAND) hc.vx = 0.3;
      if (vp.mz < -MOM_BAND) hc.vx = -0.3;
      if (vp.mx > MOM_BAND) hc.vy = 0.3;
      if (vp.mx < -MOM_BAND) hc.vy = -0.3;
      if (vp.my > MOM_BAND) hc.vz = 0.3;
      if (vp.my < -MOM_BAND) hc.vz = -0.3;
      if (hc.dax > 1.5*MAX_TRANS && hc.velx > 0.0) hc.velx = 0.0;DOIF
      if (hc.dax < -1.5*MAX_TRANS && hc.velx < 0.0) hc.velx = 0.0;DOIF
      if (hc.dax > 1.5*MAX_TRANS && hc.vely > 0.0) hc.vely = 0.0;DOIF
      if (hc.dax < -1.5*MAX_TRANS && hc.vely < 0.0) hc.vely = 0.0;DOIF
      if (hc.phl > 1.0*MAX_ANGLE && hc.vx > 0.0) hc.vx = 0.0;DOIF
      if (hc.phl < -1.0*MAX_ANGLE && hc.vx < 0.0) hc.vx = 0.0;DOIF
      if (hc.theta > 1.0*MAX_ANGLE && hc.vy > 0.0) hc.vy = 0.0;DOIF
      if (hc.theta < -1.0*MAX_ANGLE && hc.vy < 0.0) hc.vy = 0.0;DOIF
      if (hc.pai > 2.0*MAX_ANGLE && hc.vz > 0.0) hc.vz = 0.0;DOIF
      if (hc.pai < -2.0*MAX_ANGLE && hc.vz < 0.0) hc.vz = 0.0;DOIF
    }
  }
}

controller(hc)
leg1.tan.ret.cnd = v_per_pos*hc.phidot;
leg1.tan.ret.cnd = v_per_pos*hc.theta;
leg1.tan.ret.cnd = v_per_pos*hc.phidot;
leg1.lin.ret.cnd = v_per_pos*hc.ddot;
leg2.lin.ret.cnd = v_per_pos*hc.ddot;
leg2.lin.ret.cnd = v_per_pos*hc.ddot;
leg2.lin.ret.cnd = v_per_pos*hc.ddot;
/* leg1 tangential rate loop */

```



```

leg1.tan.rst.err = leg1.tan.set.cmd - leg1.tan.rst.val;
if (vp.igo == INT_ON)
    leg1.tan.rst.ier = lim(leg1.tan.rst.ier +
        DELTA*leg1.tan.rst.err, -INT_LIM, INT_LIM);
leg1.tan.mot.val = lim(vp.kr*leg1.tan.rst.ier, -VOLT_LIM, VOLT_LIM);
/* leg2 tangential rate loop */
leg2.tan.rst.err = leg2.tan.set.cmd - leg2.tan.rst.val;
if (vp.igo == INT_ON)
    leg2.tan.rst.ier = lim(leg2.tan.rst.ier +
        DELTA*leg2.tan.rst.err, -INT_LIM, INT_LIM);
leg2.tan.mot.val = lim(vp.kr*leg2.tan.rst.ier, -VOLT_LIM, VOLT_LIM);
/* leg3 tangential rate loop */
leg3.tan.rst.err = leg3.tan.set.cmd - leg3.tan.rst.val;
if (vp.igo == INT_ON)
    leg3.tan.rst.ier = lim(leg3.tan.rst.ier +
        DELTA*leg3.tan.rst.err, -INT_LIM, INT_LIM);
leg3.tan.mot.val = lim(vp.kr*leg3.tan.rst.ier, -VOLT_LIM, VOLT_LIM);
/* leg1 linear rate loop */
leg1.lin.rst.err = leg1.lin.set.cmd - leg1.lin.rst.val;
if (vp.igo == INT_ON)
    leg1.lin.rst.ier = lim(leg1.lin.rst.ier +
        DELTA*leg1.lin.rst.err, -INT_LIM, INT_LIM);
leg1.lin.mot.val = lim(vp.kr*leg1.lin.rst.ier, -VOLT_LIM, VOLT_LIM);
/* leg2 linear rate loop */
leg2.lin.rst.err = leg2.lin.set.cmd - leg2.lin.rst.val;
if (vp.igo == INT_ON)
    leg2.lin.rst.ier = lim(leg2.lin.rst.ier +
        DELTA*leg2.lin.rst.err, -INT_LIM, INT_LIM);
leg2.lin.mot.val = lim(vp.kr*leg2.lin.rst.ier, -VOLT_LIM, VOLT_LIM);
/* leg3 linear rate loop */
leg3.lin.rst.err = leg3.lin.set.cmd - leg3.lin.rst.val;
if (vp.igo == INT_ON)
    leg3.lin.rst.ier = lim(leg3.lin.rst.ier +
        DELTA*leg3.lin.rst.err, -INT_LIM, INT_LIM);
leg3.lin.mot.val = lim(vp.kr*leg3.lin.rst.ier, -VOLT_LIM, VOLT_LIM);
/* actuator commands */

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dtoa_write(card[leg1.tan.mot.crd],leg1.tan.mot.chm,VOLTRAGE,leg1.tan.mot.val);
dtoa_write(card[leg1.lin.mot.crd],leg1.lin.mot.chm,VOLTRAGE,leg1.lin.mot.val);
dtoa_write(card[leg2.tan.mot.crd],leg2.tan.mot.chm,VOLTRAGE,leg2.tan.mot.val);
dtoa_write(card[leg2.lin.mot.crd],leg2.lin.mot.chm,VOLTRAGE,leg2.lin.mot.val);
dtoa_write(card[leg3.tan.mot.crd],leg3.tan.mot.chm,VOLTRAGE,leg3.tan.mot.val);
dtoa_write(card[leg3.lin.mot.crd],leg3.lin.mot.chm,VOLTRAGE,leg3.lin.mot.val);

```

```

/* Changes: 12/21/89 DJL Moved #defines for constants and typedefs for */
/*          and references to math.h out */
/*          main. Replaced #include for math.h with */
/*          mymath.h. */
/* .....Velocity Control Subroutine and Main Driver ..... */
/* Project: Virtual Pivot Hand Controller (IBAD #4925-3000-2822) */
/* Programmed By: William C. Marshall
                Systems & Research Center
                3800 Technology Drive
                3650 Technology Drive
                Minneapolis, MN 55418
                (612) 782 - 7266
                29 Nov 1989
/* Description: Theory of the C-Language code of this subprogram is
                documented in the technical memo "Adaptable 6-DOF
                Virtual Pivot Handcontroller: System Equations",
                by W.C. Marshall, Dec 1989.
/* ..... Start of Global Declarations ..... */
#include "../include/mymath.h"
#include "../include/hct.h"
#include "gadio.h"
/* List of functions used by "main" */
void controller();
void orient();
void euler();
void quat();
void eulerf();
void matmp();
void matran();
void matinv();
void quatf();
void quatinv();
void smult();
/* MISCELLANEOUS */
static float sph3(3);
static float sph3(3);
/* Euler transformation matrix (Base-To-Platform) */
/* Euler transformation matrix (Platform-To-Base) */

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static float eh2(3){3},eh3(3){3}; /* Constant matrix sb to sli for Di(3) */
static float tmp(3); /* Temporary vector storage */

static float di,dr,d3;
static float the1,the2,the3;
static float the1,the2,the3;
static float the1,the2,the3;
static float sph1,sph2,sph3;
static float sph1,sph2,sph3;
static float the1,the2,the3;
static float the1,the2,the3;
static float did,d2d,d3d;
static float detem,temp;
static float dlo,dco,d3o,d1o,d2o,d3o;
static float the1,the2,the3;
static float the1,the2,the3;
static float wats(3);
static float pval(3);

/* .....DEDUCING DECLARATIONS..... */

static int RU000 = 1; /* -1 means set IC from pos. & angles */
static int RU001 = 1; /* -1 means print ephi(1){1} */
static int RU002 = 0; /* -1 means print phi(2){2} */
static int RU003 = 0; /* -1 means print phi(2){2},phi(3){3} */
static int RU004 = 1; /* -1 means print phi(2) & did outputs */
static int RU005 = 1; /* -1 means print V1 vectors */
static int RU006 = 1; /* -1 means print euler angles */
static int RU007 = 1; /* -1 means print (C)matrix commands/ */
static int RU008 = 1; /* -1 means print eluit matrix result */
static int RU009 = 1; /* -1 means print di,the1o,phi1o */
static int RU010 = 1; /* -1 means print di,the1o,phi1o */
static int RU011 = 0; /* -1 means print d1,the1,phi1 */
static int RU012 = 1; /* -1 means print Di(1) */

/* ===== */
fig 0
main()
{
    int j;
    struct sensor sdata;
    j = 0;

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/* Set default values */

sdata.d1 = 4.0;
sdata.ch1 = .0;
sdata.ph1 = .0;
sdata.d2 = 4.0;
sdata.ch2 = .0;
sdata.ph2 = .0;
sdata.d3 = 4.0;
sdata.ch3 = .0;
sdata.ph3 = .0;
sdata.d4 = 4.0;
sdata.ch4 = .0;
sdata.velx = .0;
sdata.vy = .0;
sdata.vx = .0;
sdata.vy = .0;

DELA(0) = .0;
DELA(1) = .0;
DELA(2) = .0;
PHIC = .1;
PHIC = .0;
PHIC = .0;

/* Set default commands if to be used */

if (BUG030>0) orient(sdata);
controller(sdata);

/* Use position & angle vectors */
/* Invoke motor velocity control */

if (BUG01>0) printf(" 01:epb(0) = %2.3f %2.3f %2.3f\n", epb(0)[0], epb(0)[1], epb(0)[2]);
if (BUG01>0) printf(" 01:epb(1) = %2.3f %2.3f %2.3f\n", epb(1)[0], epb(1)[1], epb(1)[2]);
if (BUG02>0) printf(" 02:epb(0) = %2.3f %2.3f %2.3f\n", epb(2)[0], epb(2)[1], epb(2)[2]);
if (BUG02>0) printf(" 02:epb(1) = %2.3f %2.3f %2.3f\n", epb(3)[0], epb(3)[1], epb(3)[2]);
if (BUG03>0) printf(" 03:RL, R2, R3, R4 = %2.3f %2.3f %2.3f %2.3f\n", RL(0), R2(0), R3(0), R4(0));
if (BUG03>0) printf(" 03:RL, R2, R3, R4 = %2.3f %2.3f %2.3f %2.3f\n", RL(1), R2(1), R3(1), R4(1));
if (BUG03>0) printf(" 03:RL, R2, R3, R4 = %2.3f %2.3f %2.3f %2.3f\n", RL(2), R2(2), R3(2), R4(2));
if (BUG04>0) printf(" 04:did = %2.3f %2.3f %2.3f\n", V1(0), V1(1), V1(2));
if (BUG04>0) printf(" 04:did = %2.3f %2.3f %2.3f\n", V2(0), V2(1), V2(2));
if (BUG05>0) printf(" 05:V2 = %2.3f %2.3f %2.3f\n", V2(0), V2(1), V2(2));
if (BUG05>0) printf(" 05:V2 = %2.3f %2.3f %2.3f\n", V2(1), V2(2), V2(3));
if (BUG05>0) printf(" 06:PHIC, THEC, PHIC = %2.3f %2.3f %2.3f\n", PHIC, THEC, PHIC);
if (BUG07>0) printf(" 07:PHIC, THEC, PHIC = %2.3f %2.3f %2.3f\n", PHIC, THEC, PHIC);

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if (RND009>0) printf(" 01:epoc[0][5] = %2.3f %2.3f %2.3f\n", epoc[0][0], epoc[0][1], epoc[0][2]);
if (RND009>0) printf(" 01:epoc[1][5] = %2.3f %2.3f %2.3f\n", epoc[1][0], epoc[1][1], epoc[1][2]);
if (RND009>0) printf(" 01:epoc[2][5] = %2.3f %2.3f %2.3f\n", epoc[2][0], epoc[2][1], epoc[2][2]);
if (RND009>0) printf(" 01:epoc[3][5] = %2.3f %2.3f %2.3f\n", epoc[3][0], epoc[3][1], epoc[3][2]);
if (RND009>0) printf(" 01:thec = %2.3f %2.3f %2.3f\n", thec, the2c, the3c);
if (RND009>0) printf(" 01:dic = %2.3f %2.3f %2.3f\n", dic, dic2, dic3);
if (RND009>0) printf(" 01:thai = %2.3f %2.3f %2.3f\n", thai, thai2, thai3);
if (RND010>0) printf(" 10:thai = %2.3f %2.3f %2.3f\n", thai, thai2, thai3);
if (RND010>0) printf(" 10:dic = %2.3f %2.3f %2.3f\n", dic, dic2, dic3);
if (RND010>0) printf(" 11:RNC = %2.3f %2.3f %2.3f\n", RNC[0], RNC[1], RNC[2]);
if (RND010>0) printf(" 12:DI[5] = %2.3f %2.3f %2.3f\n", DI[0], DI[1], DI[2]);
if (RND010>0) printf(" 12:DI[3] = %2.3f %2.3f %2.3f\n", DI[0], DI[1], DI[2]);
if (RND012>0) printf(" 12:DI[3] = %2.3f %2.3f %2.3f\n", DI[0], DI[1], DI[2]);

printf(" J= %3d\n", J);
scanf("%2d", &J);
return;
}

// ..... Start of Orientation Control Function ..... */

void orient(data)
struct sensor *data;
{
    int i, j;

    euler (PHIC, THIC, PSIC, epoc);

    RNC[0] = DELTA(0);
    RNC[1] = DELTA(1);
    RNC[2] = DELTA(2) - HEIGHT;

    R1B[0] = RNC[0] + RPLAT*epoc[0][0];
    R1B[1] = RNC[1] + RPLAT*epoc[0][1];
    R1B[2] = RNC[2] + RPLAT*epoc[0][2];

    R2B[0] = RNC[0] + RPLAT*(SR323*epoc[1][0] - HALF*epoc[0][0]);
    R2B[1] = RNC[1] + RPLAT*(SR323*epoc[1][1] - HALF*epoc[0][1]);
    R2B[2] = RNC[2] + RPLAT*(SR323*epoc[1][2] - HALF*epoc[0][2]);

    R3B[0] = RNC[0] + RPLAT*(-SR323*epoc[1][0] - HALF*epoc[0][0]);
    R3B[1] = RNC[1] + RPLAT*(-SR323*epoc[1][1] - HALF*epoc[0][1]);
    R3B[2] = RNC[2] + RPLAT*(-SR323*epoc[1][2] - HALF*epoc[0][2]);

    // Compute BL vectors wrt SB (BL to PL)
}

/* Compute commanded euler matrix SB to Sp) */
/* Compute position vector of platform wrt base */
/* Compute leg vectors wrt SB
*/

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D1b[0] = R1b[0] - RBASE;
D1b[1] = R1b[1] - RBASE;
D1b[2] = R1b[2];

D2b[0] = R2b[0] + HALF*RBASE;
D2b[1] = R2b[1] - SR3D2*RBASE;
D2b[2] = R2b[2];

D3b[0] = R3b[0] + HALF*RBASE;
D3b[1] = R3b[1] + SR3D2*RBASE;
D3b[2] = R3b[2];

dlc2 = .0;
for(j=0;j<3;j++) dlc2 = dlc2 + D1b[j]*D1b[j];
dsc2 = .0;
for(j=0;j<3;j++) dsc2 = dsc2 + D2b[j]*D2b[j];
dsc3 = .0;
for(j=0;j<3;j++) dsc3 = dsc3 + D3b[j]*D3b[j];

/*Compute Leg length coord. dl */

/* Rotate to Leg Base frame */

/* Compute phi & theta motor angles */

e1[0][0] = -HALF;
e1[1][0] = -SR3D2;
e1[2][0] = .0;
e1[0][1] = SR3D2;
e1[1][1] = -HALF;
e1[2][1] = .0;
e1[0][2] = .0;
e1[1][2] = .0;
e1[2][2] = 1.0;

e3[0][0] = -HALF;
e3[1][0] = SR3D2;
e3[2][0] = .0;
e3[0][1] = -SR3D2;
e3[1][1] = -HALF;
e3[2][1] = .0;
e3[0][2] = .0;
e3[1][2] = .0;
e3[2][2] = 1.0;

for(j=0;j<3;j++) d1[j] = D1b[j];
matmul(e1,d2b,d2);
matmul(e3,d3b,d3);
dlc = sqrt(dlc2);

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d2c = sqrt(d2c2);
d3c = sqrt(d3c2);

phi1c = atan2(_D1[1],d1c);
theta1 = asin(-_D1[0]/sqrt(_D1[0]*_D1[0] + _D1[2]*_D1[2]));

phi2c = atan2(_D2[1],d2c);
theta2 = asin(-_D2[0]/sqrt(_D2[0]*_D2[0] + _D2[2]*_D2[2]));

phi3c = atan2(_D3[1],d3c);
theta3 = asin(-_D3[0]/sqrt(_D3[0]*_D3[0] + _D3[2]*_D3[2]));

```

```

/* ..... */
/* Set output values */

```

```

sdata->d1 = d1c;
sdata->theta1 = theta1c;
sdata->phi1 = phi1c;
sdata->d2 = d2c;
sdata->theta2 = theta2c;
sdata->phi2 = phi2c;
sdata->d3 = d3c;
sdata->theta3 = theta3c;
sdata->phi3 = phi3c;

return;
}

```

```

/* ..... End of orient function. .... */
/* ..... Start of Velocity Control Function ..... */

```

```

void controller(sdata)
struct sensor *sdata;

```

```

{
    float dat1,dat2,dat3;

    d1 = sdata->d1;
    theta1 = sdata->theta1;
    phi1 = sdata->phi1;
    d2 = sdata->d2;
    theta2 = sdata->theta2;
}
/* Transfer input data from global storage */

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```

30  phi2 = sdata->phi2/
31  d3
32  theta3 = sdata->theta3/
33  phi3 = sdata->phi3/
34
35  vvel[0] = sdata->vvelx/
36  vvel[1] = sdata->vely/
37  vvel[2] = sdata->velz/
38
39  /*---d31---
40
41  ANOTE[0] = sdata->axr/
42  ANOTE[1] = sdata->ayr/
43  ANOTE[2] = sdata->azr/
44
45  pvel[0] = sdata->pwelx/
46  pvel[1] = sdata->pwely/
47  pvel[2] = sdata->pwelz/
48
49  wvel[0] = sdata->wvelx/
50  wvel[1] = sdata->wvely/
51  wvel[2] = sdata->wvelz/
52
53  avel = sin(theta1)/
54  avel = cos(theta1)/
55  aphi1 = cos(phi1)/
56
57  avel2 = sin(theta2)/
58  avel2 = cos(theta2)/
59  aphi2 = sin(phi2)/
60  aphi2 = cos(phi2)/
61
62  avel3 = sin(theta3)/
63  avel3 = cos(theta3)/
64  aphi3 = sin(phi3)/
65  aphi3 = cos(phi3)/
66
67  /* Compute R1,R2,R3,RP vectors */
68
69  R1[0] = -d1*avel + RMASS/
70  R1[1] = d1*avel*aphi1/
71  R1[2] = -d1*avel*cphi1/
72
73  R2[0] = d2*(HALF*avel2) - (SH3D2*cthe2*phi12) - RMA2/
74  R2[1] = d2*(-SH3D2*avel2) - (HALF*cthe2*phi12) + SH3D2*MASS/
75  R2[2] = -d2*cthe2*cphi2/
76
77  R3[0] = d3*(HALF*avel3) + (SH3D2*cthe3*phi13) - RMA3/
78  R3[1] = d3*(SH3D2*avel3) - (HALF*cthe3*phi13) - SH3D2*MASS/
79  R3[2] = -d3*cthe3*cphi3/

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/* Compute platform origin position vector */
for(j=0; j<3; j++) RP[j] = (1.0/3.0)*(R1[j] + R2[j] + R3[j]);

/* Compute euler matrix epb(l1){j} */
for(j=0; j<3; j++) RP[j] = (R1[j] - RP[j])/RPLAT;
for(j=0; j<3; j++) YP[j] = (R2[j] - RP[j])/RPLAT;
RP[0] = RP[1]*YP[2] - RP[2]*YP[1];
RP[1] = RP[1]*YP[1] - RP[2]*YP[2];
RP[2] = RP[0]*YP[1] - RP[1]*YP[2];

for(j=0; j<3; j++) epb[0][j] = RP[j];
for(j=0; j<3; j++) epb[1][j] = YP[j];
for(j=0; j<3; j++) epb[2][j] = RP[j];

/* Obtain euler matrix ebp(l1){j} */
transpose(epb,ebp);
/*
matcopy(epb,pval,vell);
*/
matcopy(epb,wrate,ANATE);
/*----d}-----*/

/* Compute leg position wrt Sp in Sb */
for(j=0; j<3; j++) R01[j] = R1[j] - RP[j];
for(j=0; j<3; j++) R02[j] = R2[j] - RP[j];
for(j=0; j<3; j++) R03[j] = R3[j] - RP[j];

/* Compute linear velocity of legs */
V1[0] = VELL[0] + (ANATE[1]*RP1[2] - ANATE[2]*RP1[1]);
V1[1] = VELL[1] + (ANATE[2]*RP1[0] - ANATE[0]*RP1[2]);
V1[2] = VELL[2] + (ANATE[0]*RP1[1] - ANATE[1]*RP1[0]);
V2[0] = VELL[0] + (ANATE[1]*RP2[2] - ANATE[2]*RP2[1]);
V2[1] = VELL[1] + (ANATE[2]*RP2[0] - ANATE[0]*RP2[2]);
V2[2] = VELL[2] + (ANATE[0]*RP2[1] - ANATE[1]*RP2[0]);
V3[0] = VELL[0] + (ANATE[1]*RP3[2] - ANATE[2]*RP3[1]);
V3[1] = VELL[1] + (ANATE[2]*RP3[0] - ANATE[0]*RP3[2]);
V3[2] = VELL[2] + (ANATE[0]*RP3[1] - ANATE[1]*RP3[0]);

/* Compute rate transform matrices */
el[0][0] = 0;
el[1][0] = -dl*etbel*ephil;
el[2][0] = -dl*etchei*ephil;
el[0][1] = -dl*etchei;
el[1][1] = -dl*etbel*ephil;

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a1[2][1] = d1*etha1*ephil;
a1[0][2] = -etha1;
a1[1][2] = ctha1*ephil;
a1[2][2] = -ctha1*ephil;

a2[0][0] = d2*(-SR3D2*ctha2*ephil2);
a2[1][0] = d2*ctha2*ephil2;
a2[2][0] = d2*ctha2*ephil2;
a2[0][1] = d2*(HALF*ctha2) + (SR3D2*ctha2*ephil2);
a2[1][1] = d2*(-SR3D2*ctha2) + (HALF*ctha2*ephil2);
a2[2][1] = d2*ctha2*ephil2;
a2[0][2] = (-SR3D2*ctha2) - (SR3D2*ctha3*ephil3);
a2[1][2] = (-SR3D2*ctha3) - (HALF*ctha3*ephil3);
a2[2][2] = -ctha3*ephil3;

a3[0][0] = d3*(SR3D2*ctha3*ephil3);
a3[1][0] = d3*ctha3*ephil3;
a3[2][0] = d3*ctha3*ephil3;
a3[0][1] = d3*(HALF*ctha3) + (SR3D2*ctha3*ephil3);
a3[1][1] = d3*(-SR3D2*ctha3) + (HALF*ctha3*ephil3);
a3[2][1] = d3*ctha3*ephil3;
a3[0][2] = (-SR3D2*ctha3) + (SR3D2*ctha3*ephil3);
a3[1][2] = (-SR3D2*ctha3) - (HALF*ctha3*ephil3);
a3[2][2] = -ctha3*ephil3;

/* Form final matrices */
matinv(e1,alinv,fdet1);
matinv(e2,a2inv,fdet2);
matinv(e3,a3inv,fdet3);

matcopy(e1in,V1,OUT1);
matcopy(e2in,V2,OUT2);
matcopy(e3in,V3,OUT3);

phid = OUT1[0];
phad = OUT2[0];
phad = OUT3[0];
dct = OUT1[1];
d3d = OUT2[1];
d3d = OUT3[1];
d3d = OUT3[2];

/* Compute ONE SET of euler angles (of 12!)
/* This set is psi,theta,phi (in order) Sb to Sp
*/
ANGLE[0] = atan2(epb[1][2],epb[2][2]);
ANGLE[1] = atan(-epb[0][2]);
ANGLE[2] = atan2(epb[0][1],epb[0][0]);

```

```

/* Transfer Output Data */
sdata->phidot = phid;
sdata->ph2dot = ph2d;
sdata->ph3dot = ph3d;
sdata->dlidot = d1d;
sdata->dl2dot = d2d;
sdata->dl3dot = d3d;
sdata->delx = RP[0];
sdata->delx = RP[1];
sdata->delx = RP[2];
sdata->phi = ANGLE[0];
sdata->theta = ANGLE[1];
sdata->psi = ANGLE[2];
return;
}

/*.....End of Velocity Control Fn.....*/

void quat(q1,q2,q3,q4, trans)
float q1,q2,q3,q4;
float trans[3][3];
{
    /*Compute new transformation matrix */
    trans[0][0] = (q1*q1 + q2*q2 + q3*q3 + q4*q4);
    trans[0][1] = 2.*(q1*q2 - q3*q4);
    trans[0][2] = 2.*(q2*q3 - q1*q4);
    trans[1][0] = 2.*(q2*q3 - q1*q4);
    trans[1][1] = (q1*q1 - q2*q2 + q3*q3 - q4*q4);
    trans[1][2] = 2.*(q3*q4 + q1*q2);
    trans[2][0] = 2.*(q3*q4 + q1*q2);
    trans[2][1] = 2.*(q3*q4 - q1*q2);
    trans[2][2] = (q1*q1 - q2*q2 - q3*q3 + q4*q4);
    return;
}

/*.....*/
void euler(phi,theta,psi,mat)

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```

float phi,the,psi;
float mat[3][3];

(
    float sphi,cphi,cthe,csai,cpai;
    /* ..... Euler Matrix Computation ..... */
    /* Compute euler rotation matrix from 100.Vert. to Body */
    the = sin(cthe);
    cthe = cos(cthe);
    psi = sin(psi);
    cpsi = cos(psi);
    sphi = sin(phi);
    cphi = cos(phi);
    mat[0][0] = cthe*cpai;
    mat[0][1] = cthe*cpai;
    mat[0][2] = -cthe;
    mat[1][0] = sphi*cthe*cpai - cphi*cpai;
    mat[1][1] = sphi*cthe*cpai + cphi*cpai;
    mat[1][2] = sphi*cthe;
    mat[2][0] = cphi*cthe*cpai + sphi*cpai;
    mat[2][1] = cphi*cthe*cpai - sphi*cpai;
    mat[2][2] = cphi*cthe;
    return;
)
/* ..... */

void matmpy(a,b,c)
/* Matrix(3x3) times vector(1x3) */
/* Calling sequence:
   float mat[3][3];
   float v[3];
   /* matmpy(ma,v,v) */
*/
float s[3][3];
float b[3];
float c[3];

{
    float t[3];
    t[0] = s[0][0]*b[0] + s[0][1]*b[1] + s[0][2]*b[2];
    t[1] = s[1][0]*b[0] + s[1][1]*b[1] + s[1][2]*b[2];
}

```

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t[2] = a[2][0]*b[0] + a[2][1]*b[1] + a[2][2]*b[2] ;
c[0] = t[0] ;
c[1] = t[1] ;
c[2] = t[2] ;
}
/* ..... End "matmul" Code ..... */

void matren(a,b,c)
/* Matrix transposition multiply */
/* Matrix (3x3) times vector (3x1) */
/* Calling sequence:
   float t[3] ;
   float v[3] ;
   float matren(m,v,v) */
float a[3][3] ;
float b[3] ;
float c[3] ;
{
    float t[3] ;
    t[0] = a[0][0]*b[0] + a[0][1]*b[1] + a[0][2]*b[2] ;
    t[1] = a[1][0]*b[0] + a[1][1]*b[1] + a[1][2]*b[2] ;
    t[2] = a[2][0]*b[0] + a[2][1]*b[1] + a[2][2]*b[2] ;
    c[0] = t[0] ;
    c[1] = t[1] ;
    c[2] = t[2] ;
}
/* ..... End "matren" Code ..... */

void matinv(a,b,det)
/* Matrix (3x3) Inverse & Determinant */
/* Calling sequence:
   float m[3][3] ;
   float det[3] ;
   float det ;
   float matinv(m,n,det) */
/* Gauss's Rule used to compute inverse.
   /* If det = 0, then inverse not returned always)
   /* If det "smaller" than "tiny", inverse not returned */
float a[3][3] ;
float b[3][3] ;

```

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float *det ;
{
    *det = a[0][0] * (a[1][1]*a[2][2] - a[1][2]*a[2][1])
          + a[1][0] * (a[2][1]*a[0][2] - a[0][1]*a[2][2])
          + a[2][0] * (a[0][1]*a[1][2] - a[0][1]*a[0][2]) ;
    if (fabs(*det)<100) return;
    temp = 1.0/(*det);
    b[0][0] = temp * (a[1][1]*a[2][2] - a[1][2]*a[2][1]);
    b[1][0] = -temp * (a[1][0]*a[2][2] - a[1][2]*a[2][0]);
    b[2][0] = temp * (a[1][0]*a[2][1] - a[1][1]*a[2][0]);
    b[0][1] = -temp * (a[0][1]*a[2][2] - a[0][2]*a[2][1]);
    b[1][1] = temp * (a[0][0]*a[2][2] - a[0][2]*a[2][0]);
    b[2][1] = -temp * (a[0][0]*a[2][1] - a[0][1]*a[2][0]);
    b[0][2] = temp * (a[0][1]*a[1][2] - a[0][2]*a[1][1]);
    b[1][2] = -temp * (a[0][0]*a[1][2] - a[0][2]*a[1][0]);
    b[2][2] = temp * (a[0][0]*a[1][1] - a[0][1]*a[1][0]);
}

/* ..... End "Matrix" Code ..... */

void mmult(a,b,c)
/* Matrix(3x3) times matrix(3x3) */
/* Calling sequence:
   float b[3][3] ;
   float c[3][3] ;
   float a[3][3] ;
   /* float c[3][3] =
   /* mmult(a,b,c) ;
   /* (a)(b) -> (c)
   */
float a[3][3] ;
float b[3][3] ;
float c[3][3] ;
{
    c[0][0] = a[0][0]*b[0][0] + a[0][1]*b[1][0] + a[0][2]*b[2][0] ;
    c[0][1] = a[0][0]*b[0][1] + a[0][1]*b[1][1] + a[0][2]*b[2][1] ;
    c[0][2] = a[0][0]*b[0][2] + a[0][1]*b[1][2] + a[0][2]*b[2][2] ;
    c[1][0] = a[1][0]*b[0][0] + a[1][1]*b[1][0] + a[1][2]*b[2][0] ;
    c[1][1] = a[1][0]*b[0][1] + a[1][1]*b[1][1] + a[1][2]*b[2][1] ;
    c[1][2] = a[1][0]*b[0][2] + a[1][1]*b[1][2] + a[1][2]*b[2][2] ;
    c[2][0] = a[2][0]*b[0][0] + a[2][1]*b[1][0] + a[2][2]*b[2][0] ;
    c[2][1] = a[2][0]*b[0][1] + a[2][1]*b[1][1] + a[2][2]*b[2][1] ;
    c[2][2] = a[2][0]*b[0][2] + a[2][1]*b[1][2] + a[2][2]*b[2][2] ;
}

```



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c[1][2] = a[1][0]*b[0][2] + a[1][1]*b[1][2] + a[1][2]*b[2][2] ;
c[2][2] = a[2][0]*b[0][2] + a[2][1]*b[1][2] + a[2][2]*b[2][2] ;
}
/* ..... End "mmult" Code ..... */

void transpose(a,b)
/* Matrix(3x3) transpose to matrix(3x3) */
/* Calling sequence:
   */
/* float a[3][3] ;
   */
/* float b[3][3] ;
   */
/* transpose(a,b) ;
   */
/* (a) ←→ (b)
   */

float a[3][3] ;
float b[3][3] ;
{
    b[0][0] = a[0][0] ;
    b[1][0] = a[0][1] ;
    b[2][0] = a[0][2] ;
    b[0][1] = a[1][0] ;
    b[1][1] = a[1][1] ;
    b[2][1] = a[1][2] ;
    b[0][2] = a[2][0] ;
    b[1][2] = a[2][1] ;
    b[2][2] = a[2][2] ;
}
/* ..... End "mmult" Code ..... */

```

```

define RPAT 2.5
define BASE 2.5
define HEIGHT 10.0
define RADDEG 57.29577951
define DEGRAD 0.01745329
define RPS 0.05
define RP02 0.0640240
define SR03 0.57735027
define RP02 RPAT*0.5
define RP02 BASE*0.5
define HALF 0.5

/* Platform radius to leg */
/* Base radius to leg */
/* Mean height of leg at 90 deg. */
/* Degrees per radian */
/* Radians per degree */
/* A unit number */
/* sqrt(3)/2 */
/* sqrt(3)/3 */

/* Leg #1 length & two angles (Input) */
/* Leg #2 length & two angles (Input) */
/* Leg #3 length & two angles (Input) */
/* Platform offset from zero position */
/* Platform roll,pitch,yaw (radians) */
/* Desired translational rates (m/sec.) */
/* Desired rotational rates (deg/sec.) */
/* Angle & leg rate commands (Output) */
/* Angle & leg rate commands (Output) */

```

```
/* Interface structure for "MandCtrl" I/O data */
```

```
typedef struct sensor
```

```

{
float d1,thet1,ph1;
float d2,thet2,ph2;
float d3,thet3,ph3;
float ddot,ddot,ddot;
float phi,thet,psi;
float wdot,wdot,wdot;
float phidot,phidot,phidot;
float phidot,ddot,ddot;
float phidot,ddot,ddot;
}

```

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/* User defines specifying type of input conversion desired. */
#define OFFSET_BINARY 0
#define VOLTAGE 1
#define CURRENT 2
#define MAX_CARDS 16

/* Each 6801's register block takes up 640 bytes.
   The register is organized as follows:
   ch1ab - oh1ab : channels 1 through 4 least significant bytes.
   */
   ch1ab - oh1ab : channels 1 through 4 most significant bytes.

struct register_format {
    unsigned char undef0;
    unsigned char ch1ab;
    unsigned char undef1;
    unsigned char oh1ab;
    unsigned char undef2;
    unsigned char ch2ab;
    unsigned char undef3;
    unsigned char oh2ab;
    unsigned char undef4;
    unsigned char ch3ab;
    unsigned char undef5;
    unsigned char oh3ab;
    unsigned char undef6;
    unsigned char ch4ab;
    unsigned char undef7;
    unsigned char oh4ab;
};

/* Data stored by driver for each card defined. */
struct card_data {
    struct register_format *reg_base;
    double range;
};

```

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#include "../include/math.h"
#define sign(x) ((x >= 0) ? 1 : -1)
#define PI 3.14159265358979323846
double atan2(y,x)
{
    double r;
    double x;
    if (x > 0) return(atan(y/x));
    if (x < 0) return(atan(y)*PI+atan(fabs(y/x)));
    if (y > 0) return(atan(y)/PI+PI/2);
    return(0);
}
double asin(a,b)
{
    double x,y;
    if (b < 0.0)
        x = -1.0;
    else
        x = 1.0;
    y = x*a;
    return(y);
}
double w/mod(a,y)
{
    double z;
    z = x/y;
    return (double) ((z - (double) (int)z)+y);
}

/* Data stored for use upon command completion. */
struct parameter_packet {
    unsigned long channel;
    unsigned long options;
    unsigned long *data0;
    unsigned long *data1;
}

/* Data defining each card group. */
struct card_data {
    struct register_format *reg_base;
    unsigned long channel_number;
    double range;
}

/* Queue format for each card group. */
struct queue_format {
    struct parameter_packet queue(queue_length);
    unsigned long queue_head;
    unsigned long queue_tail;
}

```

```

/* 8(6)math.h 1.23 88/03/03 SMI */
/*
 * Copyright (c) 1988 by Sun Microsystems, Inc.
 */
/*
 * #include <math.h>
 *
 * defines all the public functions implemented in libm.a.
 */
#include <floatpoint.h>
/* Contains definitions for types and
 * functions implemented in libm.a. */
/* 4.3 BSD functions: math.h 4.6 9/11/85 */
extern int finite();
extern double fabs(), floor(), ceil(), rint();
extern double hypot();
extern double exp(), exp2(), exp10();
extern double expm1(), expm2(), expm10();
extern double modf(), frexp();
extern double asinh(), acosh(), atanh();
extern double erf(), erfc();
extern double lgamma(), j0(), y0(), y1(), yn();
extern double sinh(), cosh(), tanh(), asin(), atan(), atan2();
extern double sin(), cos(), tan(), asint(), asost(), atanh();
extern double cbrt();
/* Sun definitions. */
enum fp_pi_type {
    /* Implemented precisions for trigonometric
     * argument reduction. */
    fp_pi_infinite = 0, /* Infinite-precision approximation to pi. */
    fp_pi_66 = 1, /* 66-bit approximation to pi. */
    fp_pi_53 = 2, /* 53-bit approximation to pi. */
};
extern enum fp_pi_type fp_pi; /* pi precision to use for trigonometric
 * argument reduction. */

```

```

35 /* Functions callable from C, intended to support IEEE arithmetic. */
    extern enum fp_class_type fp_class() ;
    extern int ilogb(), isint(), signbit() ;
    extern int isnan(), isnan(), isnormal(), iszero() ;
    extern double exp(), exp2(), expm1(), expm2(), expm2l(), expm2l2(),
    extern double logb(), logbf(), logbf(), logbf(), logbf(), logbf(),
    extern double min_subnormal(), max_subnormal(),
    extern double infinity(), quiet_nan(), signaling_nan() ;
/* Functions callable from C, intended to support Fortran. */
    extern double log2(), exp10(), exp2(), aint(), aint() ;
    extern void sincof() ;
/* Sun FUNCTIONS for C Programmers for IEEE floating point. */
    extern int ieee_flegs () ;
    extern int ieee_handler () ;
/* Single-precision functions callable from Fortran, Pascal, Module-2, etc.,
    take float* arguments instead of double and
    return FLOATFUNCTIONTYPE results instead of double.
    These functions are used to return a float function value without conversion to
    double.
    ASSIGNFLOAT is used to get the float value out of a FLOATFUNCTIONTYPE result.
    We don't want you to have to think about -feingaz.
    Some internal library functions pass float parameters as 32-bit values,
    disguised as FLOATPARAMETER. FLOATPARAMETERVALUEIN extracts the
    float value from the FLOATPARAMETER.
*/
/* m68000 returns float results in d0, same as int */
#define m68000
#define FLOATFUNCTIONTYPE int
#define ASSIGNFLOAT(x,y) return ((int x) < (int y))
#define ASSIGNFLOAT(x,y) *(&int *)(&x) = y
endif
/* sparc returns float results in %f0, same as top half of double */
#define sparc
#define FLOATFUNCTIONTYPE double

```

[illegible]


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#define ABS(x) ((x) < 0 ? -(x) : (x))
#define HUGE_VAL (infinity()) /* Produces IEEE infinity. */
#define HUGE (infinity()) /* For historical compatibility. */

#define DOMAIN 1
#define EING 2
#define ELOW 3
#define UNDERFLOW 4
#define TLOSS 5
#define TLOSS 6

struct exception {
    int type;
    char *name;
    double arg1;
    double arg2;
    double argval;
};

extern int signgam;
extern double fmod();
extern int matherr();

/* First three have to be defined exactly as in values.h including spacing! */

#define M_LJ2 0.69314718055994530942
#define M_LJ2 0.69314718055994530942
#define M_PI 3.14159265358979323846
#define M_SQRT2 1.41421356237309504880

#define M_E 2.7182818284590452354
#define M_LOG2E 1.4426950408889634074
#define M_LOG10E 0.43429448190325182765
#define M_LN10 2.30258509299404568402
#define M_LN2 1.57079632679489661923
#define M_PI_2 1.57079632679489661923
#define M_PI_4 0.78539816339744830962
#define M_1_PI 0.3183098861837907134
#define M_2_PI 0.63661977236758134368
#define M_2_SQRTPI 1.12837916709551257380
#define M_SQRT2_2 0.70710678118654752440
#define M_SQRT2 0.70710678118654752440
#define M_POLY1(x, c) (c) * (x) + (c)
#define M_POLY2(x, c) (c) * (x) + (c) * (x) + (c)
#define M_POLY3(x, c) (c) * (x) + (c) * (x) + (c) * (x) + (c)
#define M_POLY4(x, c) (c) * (x) + (c) * (x) + (c) * (x) + (c) * (x) + (c)

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#define _POLY6(x, c)  (_POLY3(x), c) * (x) + (c)[6]
#define _POLY7(x, c)  (_POLY6(x), c) * (x) + (c)[7]
#define _POLY8(x, c)  (_POLY7(x), c) * (x) + (c)[8]
#define _POLY9(x, c)  (_POLY6(x), c) * (x) + (c)[9]

/*      Deprecated functions for compatibility with past.
      Changes planned for future.
*/

extern double cabs(); /* Use double hypot(x,y)
                      /* Traditional cabs usage is confused -
                      /* it doesn't take care of one struct? */
extern double drem(); /* Use double remainder(x,y)
                      /* drem will disappear in a future release.
extern double gamma(); /* Use double lgamma(x)
                      /* to compute log of gamma function.
                      /* gamma is deprecated, use the gamma function
                      /* to appear in a future release.
extern double ldexp(); /* Use double scalbn(x,n)
                      /* ldexp may disappear in a future release
*/

#endif

```

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#include "._/include/mymath.h"

/* ..... BOWL DEMO DECLARATIONS ..... */
static double RADIUS = 6.0; /* Radius of bowl shape entered above origin */
static double ALP = 3; /* = (1/2)*PI radians or 90 deg. */
static double PID2 = 1.57079633; /* ..... */

void bowl(px,py,xbowl,ybowl,phibo,thabo,psibo)
double px,py; /* Bowl parameters -1.49<xi
double *xbowl,*ybowl,*xbowl; /* Bowl rel.coord. wrt platform coord. origin */
double *phibo,*thabo,*psibo; /* Bowl surface attitudes */
{
    double phi, the;

    phi = ALP*PX;
    the = ALP*PY;
    *xbowl = -RADIUS*sin(the)*cos(phi);
    *ybowl = -RADIUS*sin(phi);
    *psibo = RADIUS*cos(phi);
    *phibo = phi;
    *thabo = -the;
    *psibo = 0.0;
    /* ..... */
    *xbowl = RADIUS*sin(the);
    *ybowl = -RADIUS*cos(the)*sin(phi);
    *phibo = phi;
    *thabo = -the;
    *psibo = 0.0;
    /* ..... */
}

```



```

ASM      = z20
CC       = ccom -I/n/orion/entd/packages/gnu/include -x20 -x22 -x29 -x35 -x98 -x99 -x122 -x129 -x140
OPT128  = fml_128.obj wtfunc50hr.obj hnd.obj cmath.obj bowl.obj hyst.obj
LPT128  = fml_128.o wtfunc50hr.o hnd.o cmath.o bowl.o hyst.o
lib: is:lib.o:b
is:lib.o:b: $(OPT128)
lib$( is:lib.o:b $(LPT128)
.c.obj:
$(CC) $*.c
$(ASM) $*,$*=*
nm $*.asm $*.lst
.asm.obj:
$(ASM) $*,$*=*
.SUFFIXES: .obj .asm .c

```

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/*      Getargs.h      Types and defines needed for getargs
*/

#define INTEGER
#define BOOLEAN
#define CHARACTER
#define STRING
#define PROC

typedef struct
{
    unsigned    arg : 7 ; /* Command line switch */
    unsigned    type : 4 ; /* variable type */
    char        *variable ; /* pointer to variable */
    char        *errmsg ; /* pointer to error message */
} ARG;

extern int getargs();

```

```

/* this file does a complete context save of the 68881
and saves all the 68020 registers.

int_exit.h must be included at subroutine exit time
if this file is used.

asm[" MOVEM.L D0-D7/A0-A3,-(SP)"];
asm[" PSWAB -(SP)"];
asm[" TST.B (SP)"];
asm[" DC.L $7000000?"];
asm[" MOVEM PSWAB,-(SP)"];
asm[" MOVEM PCSR/PSR/PLAR,-(SP)"];
asm[" ST -(SP)"];
asm[" NOP?"];

/* bcc to null save */
/* null save */

```

```

/* this include file restores the 6881 after a context switch
It also restores all 68020 registers and does an RTE on exit.

```

```

It must be used if int_enter.h was included on entry to
the subroutine */

```

```

asm(
    TST.B    (SP),"      /* beq to null restore */
    DC.L    $6700000C");
asm(
    ADDQ.L   $2,SP);
asm(
    PRODEM   (SP)+,FPC/FPEN/FPIN");
asm(
    PRODEM   (SP)+,FPC/FPEN/FPIN");
asm(
    PRODEM   (SP)+,FPC/FPEN/FPIN");
asm(
    MOVEM.L  (SP)+,D0-D7/A0-A5");
asm(
    RTE");

```


[illegible]

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```

/* bit values for write register 11 */
/* clock mode control */
#define SCC_W11_OUT_XVAL 0x00
#define SCC_W11_OUT_TX_CLK 0x01
#define SCC_W11_OUT_BR_GEN 0x02
#define SCC_W11_OUT_DPILL 0x03
#define SCC_W11_TXC_OUT 0x04
#define SCC_W11_TXC_GEN 0x05
#define SCC_W11_TX_BR_GEN 0x06
#define SCC_W11_TX_DPILL 0x07
#define SCC_W11_TX_NTC 0x08
#define SCC_W11_TX_NTC_XVAL 0x09
/* lower byte of band rate generator time constant */
/* write register 12 */
/* lower byte of band rate generator time constant */
/* write register 13 */
/* upper byte of band rate generator time constant */
/* bit values for write register 14 */
/* also control bits */
#define SCC_W14_BR_EN 0x01
#define SCC_W14_BR_SNC 0x02
#define SCC_W14_DTR_FUNC 0x03
#define SCC_W14_DTR_FUNC_EN 0x04
#define SCC_W14_C21_LOOP 0x05
#define SCC_W14_NULL 0x06
#define SCC_W14_SEARCH 0x07
#define SCC_W14_RST_C1A 0x08
#define SCC_W14_D1C_DPILL 0x09
#define SCC_W14_SNC_NTC 0x0A
#define SCC_W14_SNC_NTC_EN 0x0B
#define SCC_W14_PM_MODE 0x0C
#define SCC_W14_UNRST 0x0D
/* external/status interrupt control */
/* bit values for write register 15 */
#define SCC_W15_2ERR_OHT 0x02
#define SCC_W15_CD_1E 0x03
#define SCC_W15_SYNC_1E 0x04

```

```

#define SCC_W13_RST 0x02
#define SCC_W13_RST_EN 0x03
#define SCC_W13_HOLD_BUR 0x04
#define SCC_W13_TX_3_BITS 0x05
#define SCC_W13_TX_4_BITS 0x06
#define SCC_W13_TX_5_BITS 0x07
#define SCC_W13_TX_6_BITS 0x08
#define SCC_W13_DTR 0x09
/* write register 6 */
/* sync char or adio address field */
/* write register 7 */
/* sync char or adio flag */
/* write register 8 */
/* transmit buffer */
/* bit values for write register 9 */
/* master interrupt control */
#define SCC_W9_VIS 0x01
#define SCC_W9_WV 0x02
#define SCC_W9_DLC 0x03
#define SCC_W9_RST 0x04
#define SCC_W9_RST_EN 0x05
#define SCC_W9_NO_RST 0x06
#define SCC_W9_CH_RST 0x07
#define SCC_W9_CH_RST_EN 0x08
#define SCC_W9_HOLD_RST 0x09
/* bit values for write register 10 */
/* also tx/rx control bits */
#define SCC_W10_6_BIT_SYNC 0x01
#define SCC_W10_LOOP_MODE 0x02
#define SCC_W10_ABORT_UND 0x03
#define SCC_W10_MARK_IDLE 0x04
#define SCC_W10_ACT_POLL 0x05
#define SCC_W10_TX_RST 0x06
#define SCC_W10_NMI 0x07
#define SCC_W10_PMI 0x08
#define SCC_W10_CNC_PRESBT 0x09

```

```

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define SOC_RMI3_CTS_IE 0x20
define SOC_RMI3_TX_UND_IE 0x40
define SOC_RMI3_BREAKE_IE 0x80
/* bit values for read register 0 */
/* tx/rx buffer status and external status */
define SOC_RMI3_RX_AVAIL 0x01
define SOC_RMI3_RXO_CNT 0x02
define SOC_RMI3_TX_EMPTY 0x04
define SOC_RMI3_TX_OVF 0x08
define SOC_RMI3_SYNC 0x10
define SOC_RMI3_CTS 0x20
define SOC_RMI3_TX_UND 0x40
define SOC_RMI3_BREAKE 0x80
/* bit values for read register 1 */
define SOC_RMI3_RXO_CNT 0x01
define SOC_RMI3_RXO_2 0x02
define SOC_RMI3_TXO_CNT 0x04
define SOC_RMI3_TXO_2 0x08
define SOC_RMI3_PAB_BAK 0x10
define SOC_RMI3_RX_OV_ERR 0x20
define SOC_RMI3_TXO_ERR 0x40
define SOC_RMI3_TXO_FRMSE 0x80
/* read register 2 */
/* interrupt vector */
/* bit values for read register 3 */
/* interrupt pending register */
define SOC_RMI3_RXO_IP 0x01
define SOC_RMI3_TXO_IP 0x02
define SOC_RMI3_RX_IP 0x04
define SOC_RMI3_TX_IP 0x08
define SOC_RMI3_A_TX_IP 0x10
define SOC_RMI3_A_RX_IP 0x20
/* read register 8 */
/* receive data register */
/* bit values for read register 10 */
/* misc status bits */
define SOC_RMI3_ON_LOOP 0x02

```

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define SOC_RMI3_LOOP_ERR 0x10
define SOC_RMI3_CTS_ERR 0x20
define SOC_RMI3_CTS_MIS 0x40
define SOC_RMI3_CTS_MIS 0x80
/* read register 12 */
/* lower byte of time constant */
/* read register 13 */
/* upper byte of time constant */
/* bit values for read register 15 */
/* external/status 16 bits */
define SOC_RMI3_RXO_CNT 0x02
define SOC_RMI3_CTS_IE 0x08
define SOC_RMI3_SYNC_IE 0x10
define SOC_RMI3_CTS_MIS 0x20
define SOC_RMI3_TX_UND_IE 0x40
define SOC_RMI3_BREAKE_IE 0x80
endif

```

```

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char prompt[11];
char cdp[256];
char soc_name[6];

```

```

/* 0x20 bytes are decoded for the bus interrupt module's registers.
   The nomenclature for the registers is as follows:
   or0 - or3 : control registers 0 through 3.
   vrs0 - vrs0 : vector registers 0 through 3.
   srr : software reset registers.
*/

struct bta_register_format
{
    unsigned char undef0;
    unsigned char or0;
    unsigned char undef1;
    unsigned char or1;
    unsigned char undef2;
    unsigned char vrs0;
    unsigned char undef3;
    unsigned char or3;
    unsigned char undef4;
    unsigned char vrs0;
    unsigned char undef5;
    unsigned char vrs1;
    unsigned char undef6;
    unsigned char vrs2;
    unsigned char undef7;
    unsigned char vrs3;
    unsigned char undef8;
    unsigned char srr;
    unsigned char undef[0x02];
};

```

```

/* Exception vector locations used. */
#define TRAP14 0x008
#define USER01 0x104
#define USER02 0x108
#define USER03 0x10c
#define USER04 0x110
#define USER05 0x114
#define USER06 0x11c
#define TIMER0 0x1b4
#define TIMER03 0x1fc
#define IPRTO_XFER 0x42
#define ICC_SP_RETURN 0x41
/* vec 0x41: icc */
/* vec 0x42: iprto */
/* vec 0x43: button 1 */
/* vec 0x44: button 2 */
/* vec 0x45: button 3 */
/* vec 0x46: button 4 */
/* vec 0x4d: timer a */
/* vec 0x4f: vms irq3 */

```

```

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asm(" MOVEM.L D0-D2/A0-A1, -(SP)");

double a,w;
int scum;
int run,ptr;
double sc,pc,so;
double ktp;
}
vp;
extern struct
{
    struct
    {
        struct
        {
            int ch1;
            int ord;
            double val;
            double cmd;
            double str;
            double str;
        }
        ret,pos,mot;
    }
    lin,rad,tenr;
}
leg1,leg2,leg3;

#define A_BASE_ADDR 0xffff000
#define A_RANGE 10.0
#define B_BASE_ADDR 0xffff000
#define B_RANGE 10.0
#define C_BASE_ADDR 0xffff000
#define C_RANGE 10.0
#define C_CHANNELS 10
#define IO_LEVEL 1
#define VME_LEVEL 6
#define VECTOR 215
#define BIN_ADDR 0xffff000
#define THREE_DOF 0
#define SIX_DOF 1
#define FOUR_DOF 1
#define RAGE_MODE 1
#define INT_OFF 0
#define INT_ON 1
#define BOWM_OFF 0
#define BOWM_ON 1
#define DELX 0.02
#define RATELIN 10.0
#define RPD 10.0
#define TAN_POL_SF 0.0175
#define TAN_POL_SF 2.35*RPD
#define TAN_POL_SF 2.35*RPD
#define LIM_POL_SF 0.167
#define LIM_POL_SF 10.0
#define MAX_TRANS 1.5
#define MAX_TRANS 1.5
#define MOM_DRAND 4.5
#define MOM_DRAND 30.0
#define V_PER_RPS 7.162
#define V_PER_RPS 10.0
#define V_PER_RPS 10.0
#define VOLZ_LIM 10.0

extern double MAX_FORCE,MAX_MOMENT;
extern double glob[500][8];

extern struct updat
{
    short fr,fz,fx;
    short ma,mg,mr;
    double w,dr,dr1,bol;
    double kp,kr;
}

```

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MOVEM, L (SP) + D0-D2/A0-A1*);
RTS*);
asm("asm("

Claims

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1. A six degree-of-freedom virtual pivot controller (10) comprising:
grip means (28) for receiving externally applied force and torque;
force and torque sensing means (34), connected to said grip means, for sensing the force and torque,
from up to six degrees-of-freedom, applied to said grip means;
first support means (30), connected to said sensing means, for supporting said sensing means;
second support means (48) for supporting said hand controller;
at least one variable-length member means (62) having a first flexible connector (32) attached to said
first support means (30) and a second flexible connector (60), attached to said second support means
(48), for variable supporting said first support means,
wherein said at least one variable-length member means comprises:
translation actuating means (36, 40) connected to said member means (62), for varying the length of
said member means;
translational sensing means (38), connected to said member means, for sensing a length of said
member means;
angular actuating means (46, 50, 52), connected to said member means, for angularly moving said
member means relative to said second support means; and
angular sensing means (44), connected to said member means, for sensing an angular position of said
member means relative to said second support means.
2. Controller according to claim 1 further **characterized** by comprising processing and control means
(12), connected to said force and torque sensing means (34), to said translational sensing means, to
said angular sensing means (38), to said translational actuating means (36, 40) and to said angular
actuating means (46, 50, 52), for receiving signals from said force and torque sensing means, said
translational sensing means and said angular sensing means, and for sending signals to said
translational actuating means and to said angular actuating means.
3. Controller according to claim 2, **characterized in that** said processing and control means (12) sends
signals to an external device (18) to be controlled by said hand controller (10), and receives signals for
the external device.
4. Controller according to claim 3, **characterized in that** any externally applied force and torque to said
grip means (28) is sensed by said force and torque sensing means (34) which in turn sends signals
indicating force and torque to said processing and control means (12) which in turn sends signals

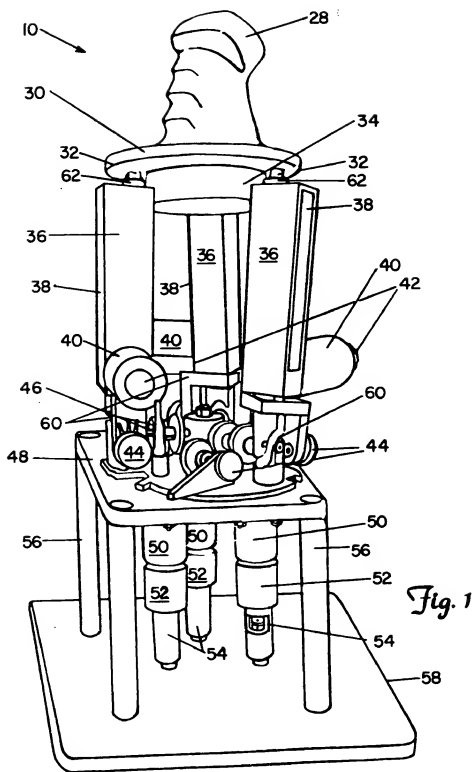
55

indicating certain kinds of control to the external device (18) being controlled which in turn sends signals of action and reflective force of the external device to said processing and control means which in turn sends signals of reflective force and movement to said translational actuating means and to said angular actuating means which in turn provide reflective force, torque and movement in response to the any externally applied force and torque to said grip means.

5 Controller according to claim 4, characterized in that said grip means (28) reflects a virtual pivot point of said grip means having to the spring-like reflective force and torque, and movement to the any externally applied force and torque.

10 6. Controller according to claim 4, characterized in that a location of the virtual pivot point and magnitudes of the spring-like reflective force and torque and of movement may be varied via input information to said processing and control means (12).

15 7. Controller according to claim 1, characterized in that said first flexible connector is a ball joint (32); said second flexible connector is a universal joint (60); said translation actuating means comprises a first motor (40), connected to said interface and control means (12), for drawing said actuating means which changes length of said variable length member (62);
20 said translational sensing means comprises:
a first tachometer (42) connected to the first motor and to said interface and control means; and
a linear potentiometer (38) connected to said linear actuator and to said interface and control means;
said angular actuating means further comprises a second motor (52), connected to said interface and control means, for driving said angular actuating means; and
25 said angular sensing means comprises:
a first angular potentiometer (44) connected to said universal joint and to said interface and control means; a second angular potentiometer (44) connected to said universal joint and to said interface and control means; and
a second tachometer (54) connected to the second motor (52) and to said interface and control means.



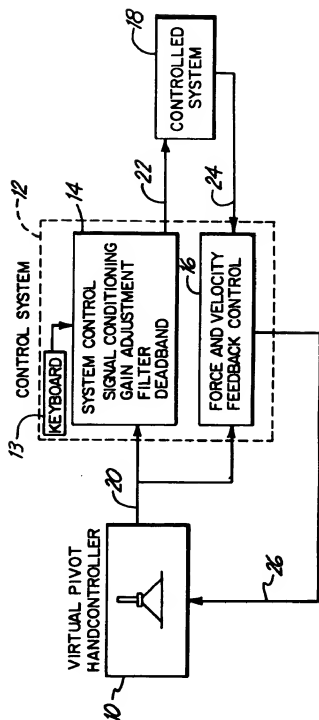


Fig. 2

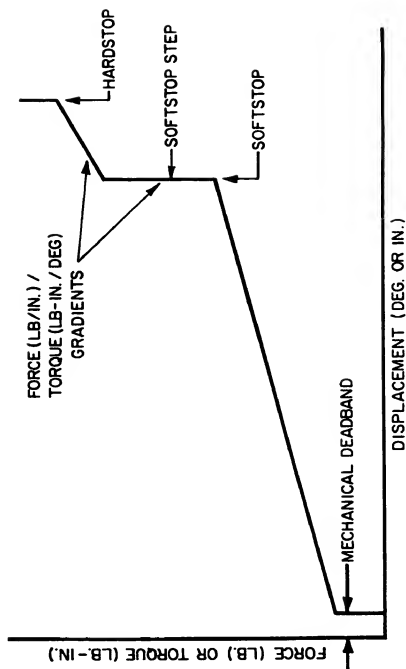


Fig. 3

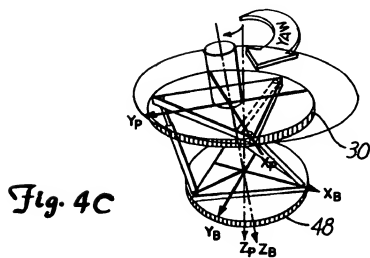
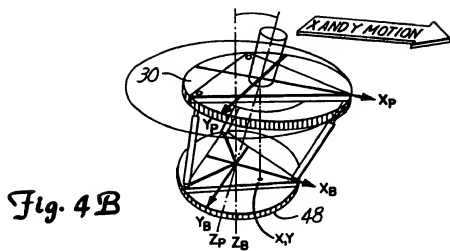
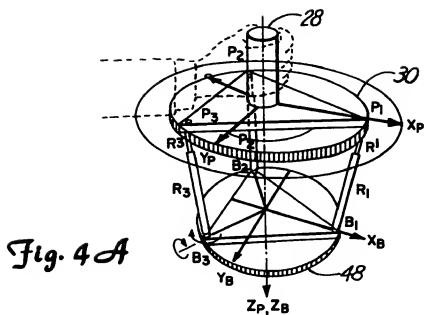
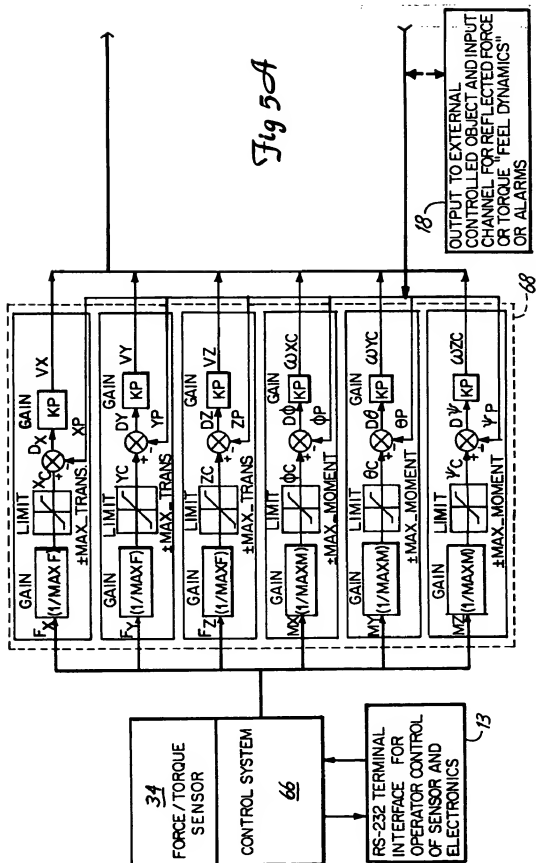
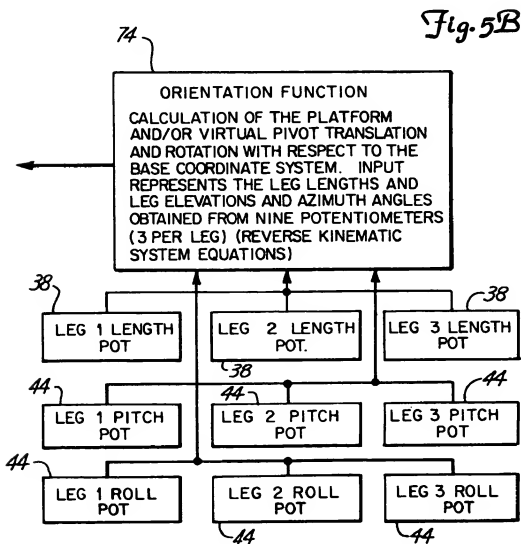
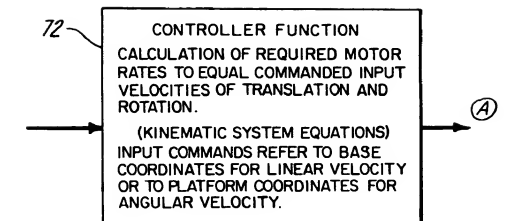


Fig 5A





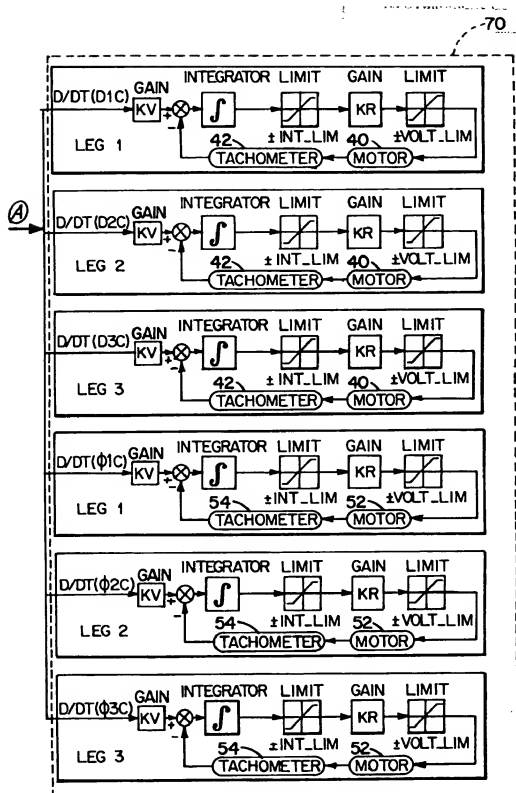


Fig. 5C



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number

EP 91 12 2237

DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	US-A-4 660 828 (WEISS) " the whole document "	1-6	G0509/04 G0505/03 G06K11/18 G06F3/033 B25J13/02
A, D	EP-A-0 363 739 (HONEYWELL) " the whole document "	1-7	
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			G01G G05G G06K G06F H01H B64C B25J
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 31 MARCH 1992	Examiner DESENA Y HERNANDOREN
CATEGORY OF CITED DOCUMENTS		Y : theory or principle underlying the invention H : earlier patent document, but published on, or after the filing date D : document cited in the application I : document cited for other reasons X : particularly relevant if taken alone V : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure F : intermediate document	
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